

2

3 Gabriel López, Christian A. Gueymard, Juan Luis Bosch, Igor Rapp-Arrarás, Joaquín Alonso-
4 Montesinos, Inmaculada Pulido-Calvo, Jesús Ballestrín, Jesús Polo, Javier Barbero. 2018.
5 Modeling water vapor impacts on the solar irradiance reaching the receiver of a solar tower
6 plant by means of artificial neural networks. Solar Energy 169, 34-39. DOI:
7 10.1016/j.solener.2018.04.023

8 Link to published version:

9 <https://www.sciencedirect.com/science/article/abs/pii/S0038092X18303682?via%3Dihub>

10

11 This is a PDF file of an unedited manuscript (post-print version) that has been accepted for
12 publication.

13

14

15

16

17

18

19

20

21

22

23

24

Modeling water vapor impacts on the solar irradiance reaching the receiver of a solar tower plant by means of Artificial Neural Networks

Gabriel López¹, Christian A. Gueymard², Juan Luis Bosch¹, Igor Rapp-Arrarás³, Joaquín Alonso-Montesinos⁴, Inmaculada Pulido-Calvo³, Jesús Ballestrín⁵, Jesús Polo⁶ and Javier Barbero⁴

¹ Dpto. Ingeniería Eléctrica y Térmica, de Diseño y Proyectos, Universidad de Huelva, Huelva (Spain)

² Solar Consulting Services, P.O. Box 392, Colebrook, NH 03576 (USA)

³ Dpto. Ciencias Agroforestales, Universidad de Huelva, Huelva (Spain)

⁴ Dpto. Química y Física, University of Almería, Almería (Spain)

⁵ Concentrating Solar System Unit (Plataforma Solar de Almería, CIEMAT), Almería (Spain)

⁶ Photovoltaic Solar Energy Unit (Renewable Energy Division, CIEMAT), Madrid (Spain)

Abstract

This work analyses the influence of water vapor on the atmospheric transmission loss of solar radiation between heliostats and the receiver of solar power tower plants. To this purpose, an atmospheric transmission code (MODTRAN) is used to generate values of direct normal irradiance (DNI) reaching the mirror and the receiver under different geometries (including sun position, tower height, and mirror-to-receiver slant range) and atmospheric conditions related to water vapor and aerosols. These variables are then used as inputs to an artificial neural network (ANN), which is trained to calculate the corresponding DNI attenuation. Two different aerosol scenarios are simulated: an ideal aerosol-free atmosphere, and a widely different one corresponding to semi-hazy conditions. The developed ANN model is then able to provide the DNI attenuation over a wide range of the input variables considered here, with root mean square differences of only 0.8%. The transmission loss due to water vapor is found to decrease with sun elevation. This is explained by the saturation effect in the incident irradiance at the mirror. The simplicity and accuracy of the algorithm are its great strengths, allowing its anticipated inclusion into the actual energy simulation codes currently used for solar tower plant design.

Keywords: solar power towers, transmission losses, water vapor, artificial neural networks

1. Introduction

Estimation of direct normal irradiance (DNI) is a research topic of increasing interest in solar energy, particularly for concentrating solar power (CSP) production. Power generation from Solar Power Towers (SPT), for which DNI is a critical input, is experiencing a rapid growth worldwide, linked to a rapid increase in the generated power and quasi-baseload opportunities offered by high-temperature heat storage. It is anticipated that the SPT technology will be one of the main contributors to the future mix of renewable energies. The greater challenges posed by these large solar installations is their complexity and cost.

65 Economies of scale are possible, but require large installations, where the outer heliostats
66 can be a few kilometers away from the receiver. To guarantee a good design and estimate of
67 the electricity production under any circumstances, it is crucial to have an accurate
68 evaluation of the DNI received by the receiver from each heliostat at any instant, since this
69 ultimately affects the operation and revenue, as well as the energy price market.

70 Under cloudless conditions, aerosols and water vapor have relatively high concentrations
71 near the ground and thus are the main variable atmospheric constituents attenuating the DNI
72 after reflection by heliostats. As a matter of fact, experience has shown that the heliostat-to-
73 tower attenuation can reach substantial levels in cases of high turbidity and/or humidity
74 content near ground level. For instance, Saharan dust outbreaks in southern Spain are not
75 rare, and produce significant attenuation levels. Figure 1 clearly illustrates the optical effect
76 of such an event, which occurred in February 2016 at the Plataforma Solar de Almería (PSA)
77 research center (Spain). That specific event and ensuing DNI attenuation are further
78 analyzed by Alonso-Montesinos et al. (2017).

79



80

81 Fig. 1: Low visibility and substantial light scattered by large particles in the atmosphere at
82 PSA on 2016-02-22 at 14:30 local time. Solar radiation reflected by the heliostats is visibly
83 attenuated by scattering.
84

85 The above-mentioned dust outbreaks occur several times a year, affecting the production of
86 all solar tower plants installed in Andalusia, in particular. Such episodes are even more
87 frequent in northern Africa, the Middle East, or Asia, where a rapid growth in the number
88 of installed SPT plants is expected. Consequently, the specialized computer codes
89 commonly used by engineers for plant sizing or energy simulation of SPT systems should
90 include the effects of these extreme atmospheric conditions, while being also flexible and
91 general in order to be used under a variety of climates, etc. Unfortunately, the models that
92 can estimate such losses were typically developed several decades ago (Vittitoe and Biggs,
93 1978; Pitman and Vant-Hull, 1982), and are insufficient to meet the increased accuracy
94 demanded by new SPT projects. Ballestrín and Marzo (2012) have compared the
95 atmospheric mirror-to-receiver (MTR) attenuation results from the above-mentioned simple
96 algorithms to detailed simulations obtained with the rigorous MODTRAN atmospheric
97 spectral code (Berk et al., 1989) for a rural-type atmosphere. Although the Pitman and Vant-
98 Hull model showed good results, both for turbid and clean conditions, only two different
99 turbidity conditions were simulated, which is far from representing all possible conditions

100 at any one SPT site.

101 In perspective, it is important to estimate the direct value of better evaluating atmospheric
102 attenuation losses. The sizing of the heliostats field using different SPT design codes such
103 as DELSOL or MIRVAL can present deviations up to 4% when considering variable
104 conditions of aerosols and water vapor, leading to significant economic repercussions
105 (Cardemil et al., 2014). Polo et al. (2017) have found differences of up to 20% in the energy
106 output production of large SPT plants depending on the time-scale input information (e.g.
107 daily, monthly or yearly values) used to model the atmospheric extinction. These findings
108 support the need of analyzing and modeling the effects of different atmospheric components,
109 such as aerosols or water vapor, on the MTR attenuation at fine temporal resolution.
110 Theoretical simulations conducted by means of spectral radiative codes, such as
111 MODTRAN, show that reductions up to 30% in solar irradiance incident on distant heliostats
112 can occur under moderately turbid conditions (López et al., 2017).

113 In recent years, methods for the direct or indirect experimental determination of the
114 horizontal extinction coefficient or of the energy attenuation have been proposed. For
115 instance, Sengupta and Wagner (2012) proposed to derive the MTR attenuation from the
116 measurement of DNI with two pyrheliometers, one measuring the incident DNI on the mirror
117 (or heliostat), and the other one measuring the DNI incident on the receiver. The authors
118 noted the great difficulties inherent to this methodology (depending on the reflectance of
119 mirrors, their cleanliness variations in local conditions, etc.), and the crucial importance of
120 measurement errors. Tahboub et al. (2014) used measurements from four pyrheliometers
121 installed on the side of a mountain and staggered at various elevations (from 340 to 1035 m)
122 to study the correlation between the DNI measurements thus obtained at different heights.
123 More generally, a thorough review of experimental methods and atmospheric attenuation
124 models can be found in the recent literature (Hanrieder et al., 2017). Even though the current
125 knowledge points at aerosols as the main source of slant MTR attenuation, there is no
126 exhaustive study analyzing the relative importance of other atmospheric variables, such as
127 water vapor, and their effects on energy losses.

128 In this work, the radiation losses specifically caused by air molecules and water vapor are
129 analyzed, and a preliminary soft-computing algorithm is proposed to evaluate them with
130 sufficient accuracy. To that end, the spectral propagation of DNI from the top of the
131 atmosphere to the receiver is simulated with MODTRAN for several air masses, also taking
132 the atmospheric composition into account. The dependence of the attenuated DNI on solar
133 zenith angle, amount of water vapor, MTR distance, and others factors, is analyzed toward
134 the development of a general prediction model.

135 Using conventional methods, the complex non-linear relationships between the various
136 atmospheric or geometric inputs and transmission loss lead to excessive difficulties in
137 finding a suitable mathematical function. An artificial neural network (ANN) is thus rather
138 developed here to obtain transmission loss estimates from the inputs considered. In addition
139 to the multiple applications of ANN methods in pattern recognition and classification,
140 function approximation, prediction, etc., their usage in data analysis is growing fast, offering
141 an effective alternative to more traditional techniques in many scientific fields. Particularly,
142 in the meteorological and solar energy resource fields, ANN-based methods have been

143 successfully developed to evaluate various solar radiation variables, thus improving their
144 accuracy with respect to more conventional statistical approaches (Bosch et al., 2008; Eissa
145 et al., 2013; López and Gueymard, 2007; Srikrishnan et al., 2015). Moreover, ANNs are
146 starting to be used to estimate solar irradiance with a similar degree of accuracy as what can
147 be achieved by the more conventional methods based on broadband or spectral radiative
148 models (Takenaka et al., 2011; Taylor et al., 2016). Thus, this emerging application of ANN
149 allows efficient (fast and accurate) calculations of the otherwise computationally expensive
150 and complex mathematical formulations involved when using conventional spectral
151 radiative transfer models.

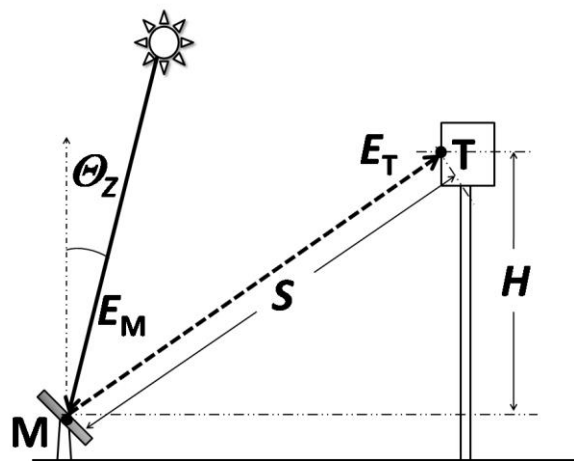
152

2. Methodology

2.1. Generation of synthetic data

153 The MODTRAN model is used here to obtain hundreds of initial predictions of the incident
154 DNI, both at the mirror M (E_M) and at the receiver on the tower T (E_T), after E_M is reflected
155 by M (Fig. 2). These simulations pertain to a large range of solar zenith angles (θ_z), mirror-
156 to-receiver slant ranges (S), tower heights (H), precipitable water (w), and two widely
157 different turbidity conditions. These initial, spectrally-based predictions are used as the
158 foundation of the proposed ANN model.
159

160



161

Fig. 2: Schematic description of the tower power plant and nomenclature.

162

163 As modeled in MODTRAN, the spectral transmittance between M and T is an intricate
164 function of line-of-sight geometry, aerosol characteristics (such as type of aerosol or type of
165 aerosol extinction), water vapor content, amounts of absorbing gases (ozone, carbon dioxide,
166 etc.), and various secondary atmospheric variables. The latter, as well as all gas amounts
167 except water vapor and carbon dioxide, are fixed here to reference values according to the
168 1976 US Standard Atmosphere (USSA). A large range of water vapor amounts is
169 considered, between 0 (ideal dry atmosphere) to 4.5 cm (subtropical conditions), including
170 the Mid-Latitude Summer (MLS) case ($w = 2.87$ cm). Additionally, the carbon dioxide
171 concentration from the original USSA (330 ppmv) is revised upward to the more current
172 value of 400 ppmv. All the other variables are varied to cover a wide range of possible
173 conditions (Table 1) and to allow comparisons with earlier studies (e.g., Ballestrín and

174 Marzo, 2012). For the latter reason, the aerosol model corresponding to the Rural extinction
 175 profile and relatively turbid conditions, represented by a surface visibility (VIS) of 23 km,
 176 is specifically selected for the present study. At the other extreme, an ideal aerosol-free
 177 atmosphere is also considered. This option is interesting since the effect of water vapor effect
 178 on the transmission loss can then be clearly identified.

179

180 Table 1: Values of the MODTRAN inputs used to obtain the simulated database.

Inputs to MODTRAN	Values
Θ_Z (degrees)	0, 10, 20, 30, 40, 50, 60, 70, 80, 85, 90
H (m)	100, 200, 250
S (km)	0.15, 0.5, 1, 2, 4
w (cm)	0, 0.25, 1.42, 2.00, 2.87, 4.50
Aerosols	No aerosols, Rural VIS = 23 km

181

182 The solar radiation reflected by the mirror M, E_M , may be obtained by MODTRAN as:

183

$$184 \quad E_M = \int_{0.28}^4 \rho_\lambda T_{\lambda M} E_{\lambda 0} d\lambda \quad (1)$$

185

186 where $E_{\lambda 0}$ is the Kurucz extraterrestrial spectral irradiance at 1 AU, $T_{\lambda M}$ is the atmospheric
 187 spectral transmittance for the sun-to-mirror path, which depends on the abundance of various
 188 atmospheric constituents, and thus varies over time, and ρ_λ is the mirror's spectral
 189 reflectance. The latter needs to be considered in order to evaluate its effect on the
 190 transmission losses of the reflected sunlight. Since this effect is relatively small, the
 191 reflectance is set here to 1 at all wavelengths for the sake of simplicity in this preliminary
 192 work. The integration limits, 0.28 μm and 4 μm , correspond to the range of wavelengths (λ)
 193 typically sensed by a pyrhelimeter. Since the attenuation due to water vapor is the only one
 194 specifically evaluated here, all other atmospheric inputs are fixed at reasonable values, as
 195 noted above. The solar zenith angle is varied incrementally from 0° to 90° as shown in Table
 196 1. Although solar power towers do not operate under large solar zenith angles, values higher
 197 than 80° are considered here anyway in order to analyze the trend of transmission losses
 198 under these extreme limits.

199 The irradiance reaching the tower receiver T (Fig. 2) is obtained using the slant-path option
 200 included in MODTRAN between two points at finite distance, i.e., the mirror and the
 201 receiver in the present case. MODTRAN calculations take into account the effects of the
 202 earth's sphericity and atmospheric refraction. The irradiance E_T is then obtained from:

203

$$204 \quad E_T = \int_{0.28}^4 \rho_\lambda T_{\lambda M-T} T_{\lambda M} E_{\lambda 0} d\lambda \quad (2)$$

205

206 where, $T_{\lambda_{M-T}}$ is the spectral transmittance for the mirror-to-tower slant path, and ρ_{λ} , T_{λ_M} and
 207 E_{λ_0} correspond to the values needed to resolve Eq. (1).

208 Since the ratio E_T/E_M represents the broadband atmospheric transmittance between M and
 209 T, the broadband atmospheric transmission loss A may be readily derived using:

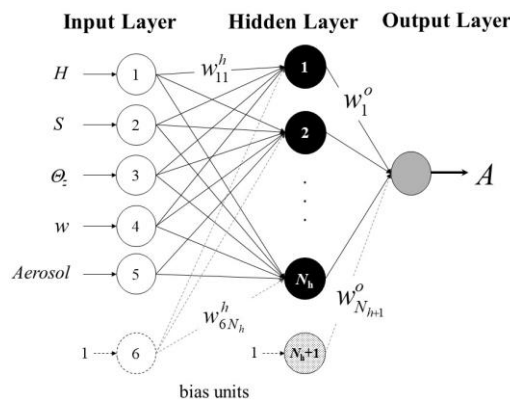
210

$$211 \quad A = 1 - E_T/E_M. \quad (3)$$

212

213 2.2. Artificial neural network

214 Artificial neural networks are implemented here using a combination of custom-designed
 215 MATLAB functions (MatLab, 1999) in conjunction with several routines developed by
 216 Nørgaard (1997). A standard multilayer perceptron (MLP) architecture with three fully
 217 interconnected layers (input, hidden, and output) is employed, as shown in Fig. 3. The
 218 hyperbolic tangent transform is chosen as the nonlinear activation function in the hidden
 219 layer, and the identity function is selected as the activation function for the output layer.
 220 Such a network determines a non-linear mapping from an input vector (constituted of the
 221 MODTRAN inputs given in Table 1) to the output, i.e., the transmission loss A . The input
 222 and output vectors are parameterized by a set of network weights. These are referred to as
 223 hidden weights, w^h (weights connecting inputs to hidden neurons), and output weights, w^o
 224 (weights connecting hidden neurons to the output one). All weights are randomly initialized
 225 within the range $(-0.5, 0.5)$. Among several existing training algorithms, a Gauss-Newton-
 226 based Levenberg-Marquardt method is selected due to its rapid convergence properties and
 227 robustness (Fletcher, 1987).



228

229 Fig. 3: Description of the ANN architecture used here.

230

3. Analysis and results

231 The influence on transmission loss of zenith angle, water vapor, and of some other variables
 232 is analyzed first. The ANN model results are presented in a second step. Figures 4 and 5
 233 show the transmission loss A versus solar zenith angle for different values of water vapor
 234 content and slant ranges, respectively for the two contrasting turbidity scenarios detailed
 235 above: an ideal aerosol-free atmosphere (Fig. 4) and semi-hazy conditions corresponding to
 236 a visibility of 23 km (Fig. 5). In both Figures the tower height is $H = 100$ m.

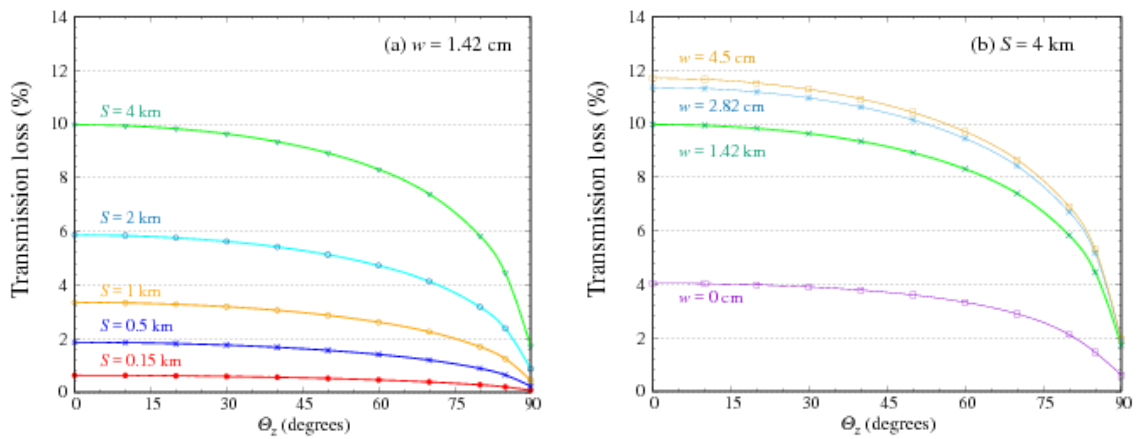


Fig. 4: Transmission loss for $H = 100$ m and an aerosol-free atmosphere, using: (a) a fixed $w = 1.42$ cm and several slant ranges, or (b) a fixed $S = 4$ km and several precipitable water values at ground level.

237

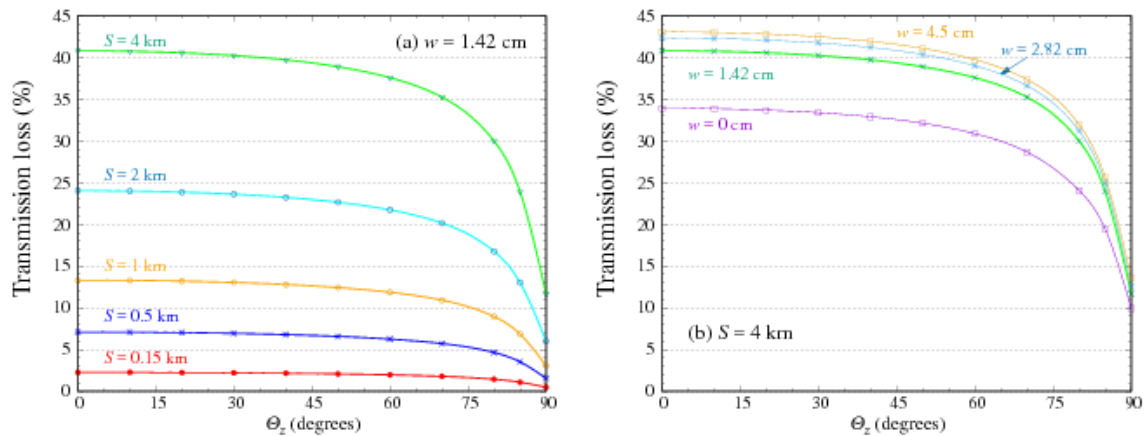
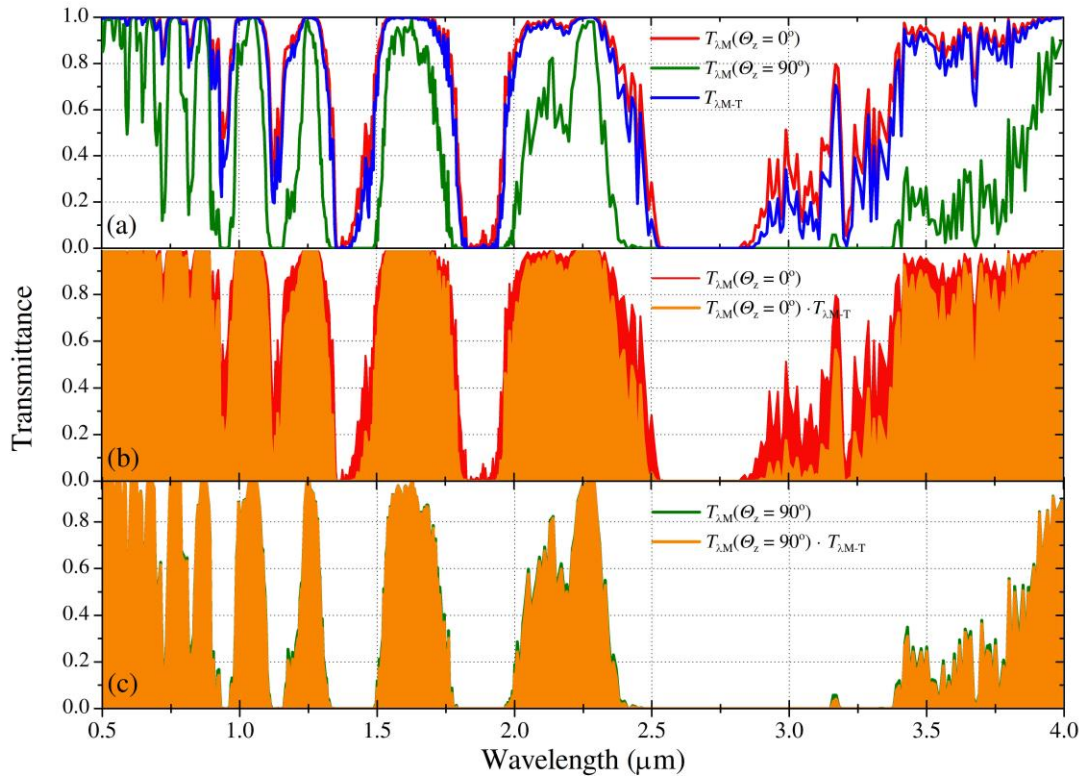


Fig. 5: Transmission loss for $H = 100$ m and semi-hazy conditions ($VIS = 23$ km), using: (a) a fixed $w = 1.42$ cm and several slant ranges, or (b) a fixed $S = 4$ km and several precipitable water values at ground level.

238 A is found to decrease sharply when zenith angle increases above $\approx 60^\circ$. More specifically,
 239 A decreases from 5.6% to 4% when θ_z increases from 30° to 70° for a medium slant range
 240 of 2 km, a constant precipitable water of 1.42 cm and an aerosol-free atmosphere. For a slant
 241 range of 4 km, this loss increases up to 9.6% for $\theta_z = 30^\circ$, or 7.3% for $\theta_z = 70^\circ$. This means
 242 that the pure effect of zenith angle is 2.3% when it varies between 30° and 70° . When haze
 243 is present (23-km visibility), this specific effect is significantly stronger, reaching 3.6% for
 244 $S = 2$ km and 5% for $S = 4$ km. On the other hand, this zenith angle effect is smaller ($\approx 1\%$)
 245 for short (< 1 km) slant ranges. The general decrease of A with increasing zenith angle is
 246 caused by the saturation effect of water vapor absorption: when θ_z increases, so does the
 247 total water vapor pathlength. This in turn depletes some wavelengths more or less
 248 completely in the water vapor absorption bands, such as around 940 nm or 1400 nm. Thus,
 249 the bulk of water vapor absorption occurs in the free atmosphere before the direct beam
 250 reaches the mirror. After reflection on the mirror, the wavelengths that were already strongly
 251 depleted before reflection cannot be depleted much more, even though there is substantial

252 water vapor between M and T. More specifically, this additional water cannot have any
253 additional effect on the strongest spectral absorption lines that are already fully saturated,
254 and can only have minimal effect on the moderately strong lines that are just partly saturated.
255 Hence, A is less intense when Θ_Z is larger, since the total water vapor pathlength is also
256 larger. Note that this saturation effect is slightly reduced if the tower height is increased,
257 because the water vapor concentration decreases with height.

258 For a better understanding of the relationship between A and sun position, Fig. 6 displays
259 the water vapor spectral transmittance corresponding to two solar positions: $\Theta_Z = 0^\circ$ and 90° .
260 Considering fixed values for the other parameters ($w = 1.42$ cm, $H = 100$ m, $S = 4$ km, and
261 aerosol-free conditions), the transmission losses are 10% and 2%, respectively (Fig. 4).
262 Figure 6a shows the spectral transmittances for each of the two path sections into which the
263 entire solar beam's pathlength can be decomposed: from the top of atmosphere (TOA) to the
264 mirror, $T_{\lambda M}$, and from the mirror to the receiver at the top of the tower, $T_{\lambda M-T}$. Fig. 6a shows
265 how the spectral transmittance along the 4-km mirror-to-receiver slant path is slightly lower
266 than that corresponding to the vertical TOA-to-mirror path ($T_{\lambda M-T} \leq T_{\lambda M}(0^\circ)$). The total
267 spectral transmittance for this case, i.e., the product $T_{\lambda M}(0^\circ) \cdot T_{\lambda M-T}$, is shown in Fig. 6b
268 (orange area). The red area corresponds to the water vapor's spectral transmittance. For this
269 example, the broadband irradiances incident on the mirror and on the receiver are
270 respectively $E_M(\Theta_Z = 0^\circ) = 1045$ W/m² and $E_T = 940.8$ W/m². A significant energy loss of
271 10% is thus obtained. In the second case, it is found that $T_{\lambda M-T} > T_{\lambda M}(90^\circ)$, as a consequence
272 of the larger sun-to-mirror path compared to the mirror-to-receiver path. The total spectral
273 transmittance for the sun-to-receiver path is $T_{\lambda M}(90^\circ) \cdot T_{\lambda M-T} \approx T_{\lambda M}(90^\circ)$. The irradiances are
274 then $E_M(\Theta_Z = 90^\circ) = 187$ W/m² and $E_T = 183.8$ W/m², leading to energy losses of about 2%.
275 This effect is similar to that corresponding to an increase the water vapor amount, as
276 explained below. The reason is that the saturation effect is driven by the total slant column
277 of water vapor, which can be approximated by $w/\cos(\Theta_Z)$ for Θ_Z less than $\approx 85^\circ$.



278

279 Fig. 6: Spectral transmittance T_λ for water vapor and different paths: (a) three paths are
 280 considered, (i) from the top of atmosphere (TOA) to the mirror at a zenith angle of
 281 0° , $T_{\lambda M}(\theta_z = 0^\circ)$; (ii) from TOA to the mirror at a zenith angle of 90° , $T_{\lambda M}(\theta_z = 90^\circ)$; and (iii)
 282 from the mirror to the receiver at the tower, $T_{\lambda M-T}$; (b) $T_{\lambda M}(\theta_z = 0^\circ)$ and the TOA-to-mirror-
 283 to-receiver path, $T_{\lambda M}(\theta_z = 0^\circ) \cdot T_{\lambda M-T}$; (c) $T_{\lambda M}(\theta_z = 90^\circ)$ and the TOA-to-mirror-to-receiver
 284 path. Aerosol-free conditions with $w = 1.42$ cm, $H = 100$ m, and $S = 4$ km are used in all
 285 cases. In the bottom panels, the colored areas under the curves describe the saturation
 286 effect of water vapor on the total transmittance. In panel (b), the red area depicts the sun-
 287 to-mirror transmittance, whereas the orange color indicates the overall sun-to-mirror-to-
 288 receiver transmittance. The mirror-to-receiver path still reduces the initial transmittance
 289 (red area). This effect is larger for wavelengths beyond $1 \mu\text{m}$. In panel (c), the orange
 290 area (similar to that for panel (b), but with $\theta_z = 90^\circ$) is almost the same as the green area,
 291 which depicts the sun-to-mirror transmittance, thus indicating that the water vapor along
 292 the mirror-to-receiver path has virtually no effect on the total transmittance.

293

294 For an ideal atmosphere without aerosols or water vapor ($w = 0$), Fig. 4 shows the non-
 295 negligible effect of Rayleigh scattering (caused by air molecules) on the reflected solar
 296 energy for $S = 4$ km, leading to transmission losses of about 4%. The dependence of A on
 297 Rayleigh scattering is almost linear with slant range, generating transmission losses of
 298 $\approx 0.15\%$ for $S = 0.15$ km, or $\approx 1\%$ for $S = 1$ km, for instance.

299 Figure 4 also shows the significant attenuation effect of water vapor on transmitted solar
 300 radiation along the mirror-to-receiver path. In an aerosol-free atmosphere, the percent
 301 energy loss due to water vapor (combined with Rayleigh scattering) can be up to 3.5% over
 302 a short slant range (1 km) and 12% for a long slant range (4 km), assuming high humidity
 303 conditions ($w = 4.5$ cm). The results in Fig. 4 indicate that, under aerosol-free conditions
 304 (where Rayleigh scattering is the only cause of attenuation, apart from absorption), A

305 increases almost linearly with slant range. The latter result is also observed under turbid
306 atmospheric conditions. Moreover, Fig. 4 reveals that the transmission loss due to water
307 vapor alone reaches $\approx 6\%$ for $S = 4$ km and low zenith angles, assuming $w = 1.42$ cm. This
308 result is similar under a semi-hazy atmosphere (Fig. 5). In contrast, when precipitable water
309 increases from 1.42 to 4.5 cm, the transmission losses only increase by 1–2%. This non-
310 linear behavior is a consequence of the strong water vapor saturation effect, as explained
311 above. This is also the reason why the transmission losses due to water vapor are relatively
312 small, even under very humid conditions ($w = 4.5$ cm), in comparison with aerosol-induced
313 losses, as the comparison of Figs. 4 and 5 reveals.

314 It is important to note that all the results above correspond to fixed rates of vertical decrease
315 (or “scale heights”) of the concentration of all atmospheric constituents, as specified by the
316 USSA or MLS reference atmospheres. In the case of water vapor close to surface level, this
317 assumed scale height is ≈ 2.2 km for USSA and ≈ 1.9 km for MLS. However, recent findings
318 using high-resolution radiosonde soundings have shown that the water vapor scale height
319 can vary rapidly (between typically 1 and 5 km) at any given site. The effect of this scale-
320 height variability on the transmission loss is not negligible, as shown by Gueymard et al.
321 (2016), and thus should be considered in future attenuation model developments.

322

323 *3.1 ANN performance*

324 To develop an ANN-based model, several free parameters must be fixed before the training
325 stage. For the MLP-based model developed here, the only free parameter is the number of
326 hidden units, N_h , since the number of inputs and outputs are fixed by design in a previous
327 step. These ANN inputs (Fig. 3) correspond to the five variables used to obtain the simulated
328 database by means of MODTRAN (Table 1): Θ_z , H , S , w and VIS. The number of hidden
329 neurons is chosen following a heuristic approach, where several networks with different
330 values of N_h are trained and the best-performing network among them is selected. For this
331 purpose, the synthetic database is randomly split into two sets, one for training the ANN and
332 the other for testing the model. The latter amounts to $\approx 10\%$ of the whole database. The ANN
333 model’s performance is analyzed in terms of both the root mean square difference (RMSD)
334 and mean bias difference (MBD) between the estimated transmission losses and the
335 MODTRAN-derived values. They are expressed as a percentage of the mean value of the
336 latter.

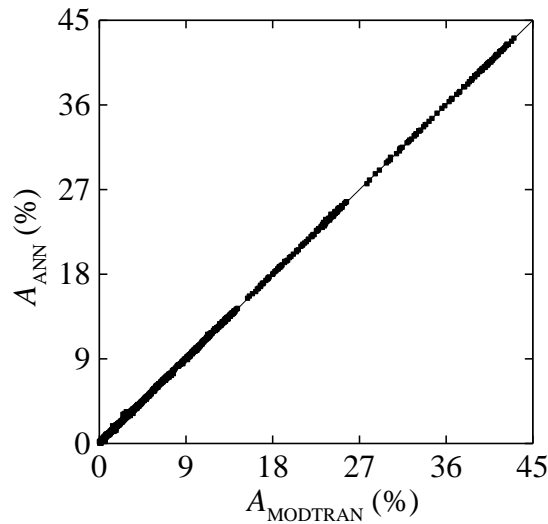


Fig. 7: Transmission loss A estimated by the ANN model compared to reference MODTRAN values.

Calculations show that the tested ANN models with $N_h > 30$ can generate very low RMSD ($< 1\%$) and no bias, whereas a low amount of hidden neurons result in a larger RMSD. N_h is thus fixed to the “optimal” value just mentioned. Figure 7 shows the transmission loss estimated by the final ANN model compared to the original MODTRAN values. An almost perfect fit is observed, with an RMSD of only 0.8%. This result demonstrates the suitability of adding an appropriate ANN-based model to SPT simulation codes, to avoid the difficulties and computer time of operating a spectral code like MODTRAN.

4. Conclusions

In this work, the energy loss of direct normal irradiance is evaluated along its path from distant mirrors to the tower receiver of a large solar tower plant, focusing on the specific impact of water vapor. It is found that the concentration of surface water vapor along the mirror-to-tower path can lead to significant reductions (up to 12%) of the solar irradiance incident on the heliostat field. It is also shown that the water vapor saturation effect limits the increase in transmission loss when water vapor reaches the high-humidity conditions typical of tropical or subtropical regions, or when zenith angle exceeds $\approx 60^\circ$. The MODTRAN simulations elaborated here further indicate that transmission losses are not constant during the day since they depend on sun position. Daily variations of $\approx 4\%$ can occur in the common operation of solar tower plants just due to this effect, at least when considering the farthest mirrors.

This contribution is apparently the first one in which the dependence of slant mirror-to-receiver attenuation on solar geometry is specifically mentioned. The analysis of an ideally pure, dry and aerosol-free atmosphere has also evidenced the non-negligible impact of molecular (Rayleigh) scattering along the mirror-to-receiver path, translating into a specific transmission loss of $\approx 1\text{--}4\%$ for far-away mirrors, which increases linearly with the slant range. All these values slightly decrease if tower height increases, as an expected consequence of the air density reduction with height.

The modeling of transmission losses using two atmospheric variables (zenith angle and

367 precipitable water) and two variables for solar power plant design parameters (slant range
368 and tower height) has been successfully solved using an artificial neural network (ANN) for
369 two contrasting atmospheric turbidity conditions. The transmission losses estimated by the
370 ANN model match those obtained by MODTRAN almost perfectly, and only require an easy
371 and fast computation. The main advantages of this ANN approach are (i) the elimination of
372 the complex and time-consuming use of MODTRAN; and (ii) the improvement in
373 transmission loss parameterization compared to what was developed empirically decades
374 ago. Thus, the present ANN model constitutes a valuable tool that could be added to existing
375 solar tower plant design and operation simulation codes. Future work will examine the
376 impact of varying vertical atmospheric profiles and different atmospheric turbidity
377 conditions, to make this ANN model even more general.

378

5. Acknowledgments

379 The authors are grateful for the financial support provided by Spanish Project PRESOL
380 “Forecast of solar radiation at the receiver of a solar power tower” with references
381 ‘ENE2014-59454-C3-1-R, ENE2014-59454-C3-2-R and ENE2014-59454-C3-3-R’, which
382 is funded by the Ministerio de Economía y Competitividad and co-financed by the European
383 Regional Development Fund.

384

6. References

- 385 Alonso-Montesinos, J., Barbero, J., Polo, J., López, G., Ballestrín, J., Batlles, F.J., 2017.
386 Impact of a Saharan dust intrusion over southern Spain on DNI estimation with sky cameras.
387 *Atmos. Environ.* 170, 279-289. <https://doi.org/10.1016/j.atmosenv.2017.09.040>.
- 388 Ballestrín, J., Marzo, A., 2012. Solar radiation attenuation in solar tower plants. *Sol. Energy*
389 86, 388–392. <http://dx.doi.org/10.1016/j.solener.2011.10.010>.
- 390 Berk, A., Bernstein, L.S., Robertson, D.C., 1989. MODTRAN: A Moderate Resolution
391 Model for LOWTRAN7. Report GL-TR-89-0122, Air Force Geophysical Laboratory,
392 Hanscom, MA.
- 393 Bosch, J.L., López, G., Batlles, F.J., 2008. Daily solar irradiation estimation over a
394 mountainous area using artificial neural networks. *Renew. Energy* 33, 1622–1628.
395 <https://doi.org/10.1016/j.renene.2007.09.012>.
- 396 Cardemil, J.M., Starke, A.R., Scariot, V.K., Grams, I.L., Colle, S., 2014. Evaluating solar
397 radiation attenuation models to assess the effects of climate and geographical location on
398 the heliostat field efficiency in Brazil. *Energy Proc.* 49, 1288–1297. doi:
399 10.1016/j.egypro.2014.03.138.
- 400 Eissa, Y., Marpu, P.R., Gherboudj, I., Ghedira, H., Ouarda, T.B.M.J., Chiesa, M., 2013.
401 Artificial neural network based model for retrieval of the direct normal, diffuse horizontal
402 and global horizontal irradiances using SEVIRI images. *Sol. Energy* 89, 1–16.
- 403 Fletcher, R., 1987. *Practical methods of optimization*. John Wiley & Sons, Chichester.
- 404 Gueymard, C.A., López, G., Rapp-Arrarás, I., 2016. Atmospheric transmission loss in
405 mirror-to-tower slant ranges due to water vapor. *AIP Conf. Proc.* 1850, 140010.

406 <https://doi.org/10.1063/1.4984518>.

407 López, G., Gueymard, C.A., 2007. Clear-sky solar luminous efficacy determination using
408 artificial neural networks. *Sol. Energy* 81, 929–939. [https://doi.org/10.1016/
409 j.solener.2006.11.001](https://doi.org/10.1016/j.solener.2006.11.001).

410 López, G., Gueymard, C.A., Bosch, J.L., 2017. Evaluation of solar energy losses for the
411 heliostat-to-receiver path of a tower solar plant for different aerosol models. *Proc. Solar
412 World Congress 2017, Abu Dhabi, UAE, International Solar Energy Society*.

413 MatLab, 1999. The MathWorks, Inc. Natick, MA, USA.

414 Hanrieder, N., Wilbert, S., Mancera-Guevara, D., Buck, R., Giuliano, S., Pitz-Paal, R., 2017.
415 Atmospheric extinction in solar tower plants – a review. *Sol. Energy* 152, 193–207.
416 <https://doi.org/10.1016/j.solener.2017.01.013>

417 Nørgaard, M., 1997. Neural network based system identification toolbox. Technical Report
418 97-E-851, Department of Automation, Technical University of Denmark.

419 Polo, P., Ballestrín, J., Alonso-Montesinos, J., López, G., Barbero, J., Carra, E., Fernández-
420 Reche, J., Bosch, J.L., Batlles, F.J., 2017. Analysis of solar tower plant performance
421 influenced by atmospheric attenuation at different temporal resolutions related to aerosol
422 optical depth. *Sol. Energy* 157, 803-810. <http://dx.doi.org/10.1016/j.solener.2017.09.003>.

423 Sengupta, M., Wagner, M., 2012. Estimating atmospheric attenuation in central receiver
424 systems. *ASME SunShot Symposium. 6th International Conference on Energy
425 Sustainability. San Diego, CA, July 23–26*.

426 Srikrishnan, V., Young, G.S., Witmer, L.Y., Brownson, J.R.S., 2015. Using multi-
427 pyranometer arrays and neural networks to estimate direct normal irradiance. *Sol. Energy*
428 119, 531–542. <https://doi.org/10.1016/j.solener.2015.06.004>.

429 Tahboub, Z., Oumbe, A., Hassar, Z., Obaidli, A., 2014. Modeling of irradiance attenuation
430 from a heliostat to the receiver of a solar central tower. *Energy Proc.* 49, 2405–2413.
431 <http://dx.doi.org/10.1016/j.egypro.2014.03.255>.

432 Takenaka, H., Nakajima, T.Y., 2011. Estimation of solar radiation using a neural network
433 based on radiative transfer. *J. Geophys. Res.* 116, D08215, 1–26.
434 [doi:10.1029/2009JD013337](https://doi.org/10.1029/2009JD013337).

435 Taylor, M., Kosmopoulos, P.G., Kazadzis, S., Keramitsoglou, I., Kiranoudis, C.T., 2015.
436 Neural network radiative transfer solvers for the generation of high resolution solar
437 irradiance spectra parameterized by cloud and aerosol parameters. *J. Quant. Spectr. Rad.
438 Transf.* 168, 176–192. <http://dx.doi.org/10.1016/j.jqsrt.2015.08.018>.

439 Vittitoe, C.N., Biggs, F., 1978. Terrestrial propagation loss. *Proc. ASES Solar
440 Diversification Conf., Denver (CO, USA)*.

441