

1 **Long term fluctuations of groundwater mine pollution in a sulfide mining district with**
2 **dry Mediterranean climate: implications for water resources management and**
3 **remediation**

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16 **Abstract**

17 Water resources management and restoration strategies, and subsequently ecological and
18 human life quality, are highly influenced by the presence of short and long term cycles
19 affecting the intensity of a targeted pollution. On this respect, a typical acid mine drainage
20 (AMD) groundwater from a sulfide mining district with dry Mediterranean climate (Iberian
21 Pyrite Belt, SW Spain) was studied to unravel the effect of long term weather changes in
22 water flow rate and metal pollutants concentration. Three well differentiated polluting
23 stages were observed and the specific geochemical, mineralogical and hydrological
24 processes involved (pyrite and enclosing rocks dissolution, evaporitic salts precipitation-
25 redissolution and pluviometric long term fluctuations) were discussed. Evidencing the
26 importance of including longer background monitoring stage in AMD management and
27 restoration strategies, the present study strongly advise a minimum 5-years period of AMD
28 continuous monitoring previous to the design of any AMD remediation system in regions
29 with dry Mediterranean climate.

30

31 **Capsule Abstract**

32 Acid mine drainage management and remediation is shown to be highly dependent of the
33 short- and long-term weather cycles affecting the intensity of this pollution.

34 **Keywords**

35 Acid mine drainage, evaporitic salts, passive treatment systems, climate change

36 **1. Introduction**

37 Acid mine drainage is the term conventionally used to refer the metal pollution and
38 physico-chemical behavior characterizing waters that have been in contact with acidity

39 producing minerals (e.g., sulfides or Fe oxides and hydroxides) in mining districts. These
40 waters exhibit several peculiarities, viz: high metal and sulfate concentration, low pH
41 values and to be commonly buffered by the precipitation of Fe (e.g., schwertmannite) or Al
42 (e.g., hydrobasaluminite) minerals (Bigham and Nordstrom 2000). Moreover, AMD
43 pollution is a worldwide and recalcitrant environmental problem affecting both surface
44 waters and groundwater that typically endures for centuries or even millennia (Younger et
45 al. 2002)).

46 AMD hydrochemistry might be significantly influenced by seasonal fluctuations
47 (Cánovas et al. 2008). Therefore, it is reasonable to expect serious effects of climate change
48 in AMD pollution that are difficult to predict (Nordstrom 2009). The effect of seasonal
49 variations in the pollution of surficial AMD has been widely studied, revealing a clear
50 correlation between drought/wet periods and AMD metal concentration. In this regard, it
51 has been repeatedly documented that the first storm event after a drought period induces a
52 sudden increase in surficial AMD acidity and metal load (Nordstrom 2009, Kimball et al.
53 2007, MacCausland and McTammany 2007, Cánovas et al. 2010). This effect has also been
54 reported as “first flush” and it is attributed to the dissolution of the efflorescent salts that
55 typically cover riverbanks during the dry season. The following storm event of the wet
56 season commonly produces a slight dilution in metal concentration and a pH increase,
57 slightly improving water quality (Cánovas et al. 2010). These seasonal variations can also
58 be recorded as sequences of precipitates within the sediments of AMD affected rivers
59 (Caraballo et al., 2011)

60 The aforementioned “first flush” concept is also applied to groundwater emerging to the
61 surface during the first months following the closure and subsequent flooding of an

62 underground mine (Gzyl and Banks, 2007; Younger, 1997). Most research effort has been
63 placed on the study of AMD groundwater in coal mining districts (Jarvis et al., 2006;
64 Lambert et al., 2004; Younger, 2000; Younger et al., 2002; and papers therein). Whereas
65 only a few studies have looked into groundwater hydrochemical variations in sulfide
66 mining districts (Gray 1998, Nordstrom et al. 2000). In coal districts, the longevity of the
67 “first flush” effect or “vestigial acidity” in the galleries has been estimated to be around 40
68 years, while the persistence of “juvenile acidity” (due to the dissolution of all the remaining
69 pyrite in the galleries) could extent along hundreds of years (Younger, 1997 and 2000). The
70 acidity and metal concentration of the AMD emerging from coal underground mines has
71 been observed to decrease with the time elapsed since the mine closure. This knowledge is
72 essential to design rational planning for the remediation of this devastating pollution.

73 On the other hand, AMD pollution in sulfide mining districts is commonly more severe
74 in terms of metal concentration and most importantly in terms of its longevity (Bigham and
75 Nordstrom 2000). This extreme longevity is due to the enormous amount of pyrite and
76 other sulfides remaining in the galleries of the abandoned mines. In some sulfide mine
77 districts, like the Iberian Pyrite Belt (IPB, SW Spain), the emerging waters from the
78 underground mines correspond to almost 40% of the AMD discharges catalogued in the
79 region (Sánchez-España et al. 2005). A good understanding of both seasonal variations and
80 inter-annual drought and flood events on AMD hydrochemistry is crucial to estimate the
81 intensity and evolution of this pollution and, subsequently to design efficient remediation
82 strategies to accommodate all the system fluctuations over time.

83 The current research analyzes the results obtained after more than 4 years monitoring the
84 emerging waters from the adit of an abandoned underground pyrite mine. The relationship

85 between the local rainfall regime and weather, the flow rate at the adit and the evolution of
86 AMD metal load is discussed. Galleries at abandoned mines are typically inaccessible, so
87 the geochemical and mineralogical processes occurring within them need to be inferred
88 only by the study of the outflowing AMD. To offer some tools enabling a realistic
89 interpretation of such hidden processes, a set of meteorological, hydrogeochemical and
90 mineralogical parameters were combined using various analytical techniques.

91

92 **2. Methods and sampling procedure**

93 *2.1. Site location*

94 The current study was performed in Mina Esperanza, located in the northern part of the
95 IPB in South-western Spain (37°45'34''N-6°41'00''O). The mineralization at Mina
96 Esperanza consists of a massive pyrite deposit with minor amounts of chalcopyrite (Pinedo-
97 Vara, 1963). The enclosing rocks are slates and low grade metamorphic phyllites. The
98 underground works mined a massive pyrite deposit with chalcopyrite, sphalerite and galena
99 (Pinedo-Vara, 1963). The mine was under operation during the first half of the last century.
100 After closure in 1975, the abandoned mine was naturally flooded and, subsequently,
101 polluted water began to flow out of the main adit. As an orphan mine site, there is not any
102 mining company liable for the generated pollution and the mining information available
103 (e.g., underground plans and drawing) is limited or entirely inexistent.

104 The pluviometric data were provided by the Spanish Weather Service
105 (<http://www.aemet.es>) and correspond to the automatic station located in El Campillo, 10
106 km apart from the Mina Esperanza mining area.

107

108 2.2. Water sampling and analyses

109 Water samples and flow measurements were taken at least twice a month from March
110 2007 to October 2008, once every 2 month from November 2009 to January 2011 and at
111 least once a month from February 2011 to June 2011. Sampling gap between November
112 2008 and October 2009 was due to logistic problems (impossibility to access the sampling
113 point). The samples were filtered immediately after collection through 0.1 μm Millipore
114 filters on Millipore syringe filter holders, acidified in the field to $\text{pH} < 1$ with Suprapur[®]
115 HNO_3 and stored at 4 °C in 60 mL sterile polypropylene containers until analyzed.

116 Temperature and electrical conductivity were measured using a portable CM35 meter
117 (Crison[®]) with 3 point calibration (147 and 1413 $\mu\text{S}/\text{cm}$ and 12.88 mS/cm). The pH and
118 redox potential were measured using a PH25 meter (Crison[®]) with Crison electrodes.
119 Redox potential and pH were controlled and calibrated using 2 points (240–470 mV) and 3
120 points (pH 4.01–7.00–9.21), respectively, with Crison[®] standard solutions. Redox potential
121 measurements were corrected to the Standard Hydrogen Electrode to calculate pe.

122 In order to obtain a better understanding of the different processes controlling the
123 outflowing water chemistry, a representative sample from the final period of study was
124 submitted to an evaporation process. The hydrochemistry evolution during the evaporation
125 process and the evaporitic salts generated were analyzed in detail. In addition, the
126 evaporation process was reproduced and studied by means of a geochemical model. A
127 detailed description of the evaporation experiment and modeling is offered in the
128 supplementary information.

129 The concentration of dissolved Fe, Cu, Zn, Na, Al, Ca, Mg, and S in solution was
130 measured by Inductively Coupled Plasma Atomic Emission Spectrometry (ICP-AES) with
131 detection limits of 10 µg/l for Fe, Cu and Zn, 100 µg/l for Na and 50 µg/l for Al, Ca, Mg
132 and S. The concentrations of As, V, Sr, Cd, Pb, Ni and Co were determined by Inductively
133 Coupled Plasma Atomic Mass Spectroscopy (ICP-MS). The detection limits were in the
134 order of 1 µg/l. In the analyses of ICP-AES and ICP-MS, calibration with sets of standards
135 was performed when the regression coefficient exceeded 0.999. Three laboratory standards
136 were analyzed within every 10 samples to check for accuracy. In the analyses of ICP-AES
137 and ICP-MS, dilutions from 1:2 to 1: 100 were performed to ensure that the concentration
138 of the samples was within the concentration range of the standards.

139 Fe(II) and total Fe were determined by colorimetry at 510 nm after complexation in the
140 field by the addition of 0.5% (w/w) 1,10-phenanthroline chloride solution to the filtered
141 sample (Rodier et al., 1996), using a DR/890 portable colorimeter (HACH®). The detection
142 limit was 0.3 mg/L and precision was better than 5%; Fe(III) was calculated as the
143 difference between total Fe and Fe(II).

144 X-ray Diffraction (XRD) of randomly oriented powder samples was obtained on a
145 Bruker D5005 X-ray diffractometer with CuK α radiation. The samples were scanned from
146 0 to 60 degrees 2 θ with a continuous scan at a rate of 0.025°/18 s.

147 Selected carbon coated samples of precipitates were observed under Scanning Electron
148 Microscopy and Microanalysis (SEM-EDS) to determine the major chemistry, morphology
149 and the sequence of formation of the precipitates from evaporation.

150

151 2.3. Statistical multivariate analyses

152 The results of the water chemical analyses and physical-chemical parameters were
153 processed using the programs XLSTAT-Pro v.5.1. Principal Component Analysis (PCA), is
154 a multivariate statistical techniques that allows a large set of data to be simplified and
155 reduced into a smaller number of orthogonal factors (with magnitude and accuracy) to
156 facilitate interpretation by visualizing the correlations that exist between the original
157 variables (Jolliffe, 2002). A PCA was carried out by means of a Spearman's correlation
158 matrix (0.05 significance level, 2 tailed test) to the variables and samples in order to
159 establish possible relations among polluting elements and also to obtain a better
160 understanding of some of the main processes involved in the groundwater pollution and
161 evolution. Due to the high correlation typically showed between dissolved metals and
162 generating processes in AMD environments, only loadings above 0.7 for the new factors
163 generated have been discussed.

164

165 2.4. Geochemical modeling

166 Water speciation and mineral saturation indexes were calculated with PHREEQC code,
167 version 2.18.00 (Parkhurst and Appelo, 1999). Thermodynamic data for minerals were
168 obtained from the WATEQ4f database (Ball and Nordstrom, 1991), except for hexahydrite
169 (Delany and Lundeen, 1990), halotrichite (Reardon, 1988), szomolnokite (Tosca et al.,
170 2005) and schwertmannite (Caraballo et al., 2013). The evaporation experiment of the
171 present study was modeled using the Pitzer ion-interaction approach. For more information
172 about the evaporation model the reader is referred to the supplementary information.

173 3. Results

174 3.1. Local climate and adit hydraulic response to the rainfall

175 The climate in the province of Huelva can be considered as dry Mediterranean type and
176 it is characterized by well-defined dry and wet seasons. Moderate changes can be observed
177 in the climate of the region between hydrological or water years (water years are considered
178 from 1st October of the past year to 30th September of the current year). To illustrate these
179 subtle variations, a decade (2001-2011) of rainfall and temperature records from El
180 Campillo weather station will be summarized. The mean yearly-accumulated rainfall during
181 that decade was around 770 mm with maximum and minimum yearly-accumulated rainfall
182 of 1,223 mm and 401.8 in 2010 and 2005, respectively (Table 1). The mean yearly-
183 temperature (calculated from mean daily-temperatures) oscillated between 16.6 and 17.5
184 while the maximum and minimum daily values recorded correspond to 43.1 (1st August
185 2003) and -2.4 (27th January 2005). The calculated standard deviations for each year mean
186 temperature ranged 5.9-7.4, showing that the oscillation between winter and summer mean
187 temperatures is not too drastic (Table 1).

188 A detailed observation of the trends shown by both rainfall and water discharged from
189 the adit (from March 2007 to August 2011) is offered in figure 1. As can be observed, there
190 is an unequivocal connection between both parameters that is characterized by a poor and
191 steady discharge during the water years with low to moderate rainfalls (2007 and 2008) and
192 by higher discharges and bigger fluctuations during water years affected by important
193 rainfalls (2010 and 2011). The underground network of tunnels and shafts in Mina
194 Esperanza can be understood as a dual porosity aquifer. In accordance to that, a delay
195 between the increase in the accumulated rainfall and its response in the adit discharge can
196 be observed (i.e., December-March 2009-10 and 2010-11, Fig. 1).

197

198 3.2. Evolution of the water chemistry

199 Some representative parameters of the adit hydrochemistry for the period 2007-2011 are
200 presented in Figure 2. Within this four-year period, three well-differentiated stages can be
201 observed. A first stage characterized by a steady metal concentration coupled to a constant
202 and low adit outflow (March 2007 to October 2008, Fig. 2). During the final period of this
203 stage, some elements like Fe or As exhibited an increasing tendency whereas the pH values
204 showed a decreasing trend.

205 The second stage covers from November 2009 to July 2010 (Fig. 2). During this time the
206 adit outflow continuously increased, as a response to the intense rainfall received by the
207 region, until reaching a maximum value (4.6 L/s) ten times higher than initial flow rate (0.4
208 L/s, Fig. 2). This gradual and severe outflow rise induced a substantial increase in the metal
209 load of these waters. Within the general increase-decrease cycle shown by the AMD
210 concentration, two different and overlapping behaviors can be differentiated. A common
211 response was observed for some mayor and minor elements like Fe and As (Fig. 2) and
212 other trace metals like V or Ti (Table A1, supplementary information). These elements
213 displayed their maximum values during the sampling on January 2010 (adit discharge = 2.5
214 L/s) and preceding the peak of maximum adit outflow (19th March 2010). On the other
215 hand, some other elements like Al, Cu and Zn (Fig. 2) and also Ca, Cd, Co, Cr, Cu, Mg,
216 Mn, Ni, SO₄ and Sr (Table S1) displayed their maximum concentrations matching the adit
217 maximum discharge. This group of elements can be typified by the behavior of Al and
218 therefore will be referred now on as the Al-group.

219 The third and final stage covers from July 2010 to June 2011 (Fig. 2). This period was
220 characterized by an increase-decrease cycle of the adit outflow. However, this cycle had a
221 negligible effect on the water metal load and hydrochemistry.

222 The Fe(II)/Fe(III) speciation was only measured during the second and third stages. Most
223 of dissolved iron is Fe(II), being the Fe(II)/FeT ratio within 0.92 and 0.98.

224

225 **4. Discussion**

226 *4.1. AMD hydrochemical response to inter annual climatic fluctuations*

227 The Fe/S_{molar} ratio is typically used to infer the extent of the control exerted by pyrite and
228 Fe-sulfates dissolution on AMD hydrochemistry (Cánovas et al., 2010; Sarmiento et al.,
229 2009 and 2011). During the first stage, the adit effluent showed a quite stable metal
230 pollution without marked seasonal variations. The Fe/S ratio increased from 0.3 to the
231 proximity of the theoretical 0.5 value assumed for pure pyrite dissolution (Fig. 3). Ferrous
232 iron oxidation and the subsequent Fe(III) minerals precipitation may account for the
233 observed Fe/S values lower than 0.5. In fact, if these waters are modeled assuming a value
234 of 0.02 for the Fe(III)/Fe_{total} ratio (the lowest value recorded at Mina Esperanza),
235 schwertmannite and jarosite-group minerals are shown to be supersaturated. AMD
236 evaporation and the concomitant precipitation of melanterite can also be responsible for
237 Fe/S values lower than 0.5.

238 The possible effects of seasonal variations in AMD can be targeted using the Zn/Cu_{molar}
239 ratio (Gray 1998, Alpers et al. 1994, Cravotta 1994). The observed correlation between
240 high Zn/Cu_{molar} values and drought periods (or between low Zn/Cu_{molar} values and wet

241 periods) has been attributed to the preferential Cu uptake (or release) during the
242 precipitation (or dissolution) of melanterite (Alpers et al. 1994). As expected, the specially
243 dry and hot conditions during the summer of 2007 led to an important increase in the
244 Zn/Cu_{molar} values (Fig. 3). On the other hand, a significant decrease in the Zn/Cu_{molar} ratio
245 was recorded coupled to the flow rate increment around May 2008, and followed by a
246 gradual increase of this ratio in the succeeding dry months (Fig. 3).

247 To untangle the different geochemical and mineralogical processes generating the
248 hydrochemical response of the second stage, it was decided to submit the results to a PCA
249 statistical multivariate analysis. As can be observed in figure 4A, 96.5% of the original
250 variance in the dataset can be represented by 2 factors. The first principal factor (F1) is by
251 far the predominant one and accounts for 81.9% of the variance, while the second one (F2)
252 only explains 14.6%. F1 loading factors are always higher than 0.7 and in many cases even
253 higher than 0.95 (Table A2, supplementary information). The first factor can be assigned to
254 the general increase-decrease cycles observed (Fig. 2 and 4A). Whereas the second factor
255 could be attributed to the well-know control exerted by pH and pe in AMD environments.
256 A detailed inspection of the PCA plot confirmed the existence of two different groups
257 already proposed in the results section (Fig. 4A): pe-group (pe, Fe(II), Fe(III), As, Ti and
258 V) and Al-group (Al, Ca, Cd, Co, Cr, Cu, Mg, Mn, Ni, S, Sr and electrical conductivity).
259 The almost symmetrical positions for pH and pe-group in the PCA plot and the high inverse
260 correlation coefficients observed (pH-pe = -0.80, Table A4, supplementary information) are
261 the typical statistical signs shown by an AMD controlled by pyrite dissolution (Cánovas et
262 al. 2010, Sarmiento et al. 2009). On the other hand, the Al-group is located almost on the
263 same place than the discharge (Q, Fig. 4A) and shows a negligible influence of F2

264 (loadings factors for F2 lower than 0.14, Table A2, supplementary information). This group
265 could be assigned to the dissolution of evaporitic salts in the galleries as a result of the adit
266 flow rate increase.

267 For the sake of clarity, the most plausible sequence of events generating the second stage
268 response will be presented. As already discussed for stage 1, AMD primary source of iron
269 (as ferrous iron) corresponds to the dissolution of pyrite within the galleries (Fig. 4B). As
270 soon as the outflow registered a significant increase in January 2010, both Fe(II) and Fe(III)
271 showed their maximum concentrations (Fig. 4B) due to the combination of an increase in
272 pyrite dissolution (new sources of pyrite are accessible because of the water table rise) and
273 the dissolution of evaporitic salts (mainly melanterite, an extra source of ferrous iron) and
274 schwertmannite/jarosite (source of ferric iron, Fig. 4B). Pursuant to the evaporation
275 experiment performed to the AMD at Mina Esperanza (supplementary information), a
276 sequential precipitation of evaporitic salts beginning with gypsum, CaSO_4 , followed by
277 melanterite, FeSO_4 , and finally alunogen, $\text{Al}_2(\text{SO}_4)_3 \cdot 17\text{H}_2\text{O}$, is expected. As the adit
278 discharge increase, the underground water reached new regions of the galleries continuing
279 the dissolution of the sequence of evaporitic salts. As a result, the asynchrony between the
280 maximum peaks of pe- and Al- groups was observed (Fig. 2). This sequential evaporitic
281 salts dissolution event is supported by both Fe/S and Zn/Cu molar ratios. As shown in
282 figure 3, as soon as the adit discharge increased (January 2010) the Zn/Cu ratio suffered a
283 pronounced decrease, marking the beginning of the evaporitic salts dissolution. However,
284 the Fe/S ratio showed its maximum drop only after the most intense dissolution of non-iron
285 evaporitic salts (coincident with the Al-group peak) began in March 2010. Once the
286 evaporitic salts were washed out and the adit flow rate began to decrease, Mina Esperanza

287 AMD progressively resumed its characteristic metal load (Fig. 2) and Fe/S and Zn/Cu ratios
288 (Fig. 3).

289 The main characteristic defining the third stage is the absence of any significant metal
290 concentration peak despite the existence of an important discharge peak (Fig. 2). However,
291 two synchronous and small decreases in Fe/S and Zn/Cu molar ratios were detected on
292 February 2011 (Fig. 3). This observation suggests the possible redissolution of the evaporitic
293 salts precipitated during the 2 or 3 months of lower flow rate in the transition from stage 2
294 to stage 3.

295 4.2. Implications for AMD management and remediation

296 The hydrochemistry and flow rate of the AMD emerging from the adit of Mina
297 Esperanza can be considered as representative of a high polluted AMD in the IPB
298 (Sánchez-España et al., 2005; Sarmiento et al., 2009). In this regard, the three different
299 stages categorized in the present study could be used as valuable background information to
300 design AMD management and remediation plans. This information is not only relevant for
301 the IPB but also to many other AMD affected mine districts with dry Mediterranean climate
302 around the world, such as in California (Druschel et al., 2004), Western Australia
303 (Biermann et al., 2014), North Africa (Hakkou et al., 2008) and Middle East (Gemici, U.,
304 2008).

305 Several routine operational parameters (employed in the design of AMD remediation
306 strategies) will be briefly defined to facilitate the discussion in this section. Net acidity (*NA*,
307 g/L as CaCO₃ equivalents) was calculated using the following equation after Kirby and
308 Cravotta (2005):

$$NA = 50.045 \cdot (3 \cdot c_{Al} + 2 \cdot c_{Fe} + 2 \cdot c_{Mn} + 2 \cdot c_{Zn} + 10^{-pH}) - alk \quad (1)$$

309 where c_i is the molar concentration of the i th metal (mol/L), alk is the measured gross
 310 alkalinity (mg/L as CaCO_3 equivalents) and 50.045 converts moles of charge into grams of
 311 CaCO_3 equivalents. This parameter can be understood as the AMD potential to generate
 312 acidic conditions. Net acidity load (NAL , kg/day as CaCO_3 equivalents) offers an idea of
 313 the “working load” that a remediation system will have to face. In other words, it is an
 314 estimation of the net acidity that needs to be neutralized per day. It was generated according
 315 to the following equation:

$$NAL = NA \cdot Q \quad (2)$$

316 where NA is given in kg/L as CaCO_3 equivalents and Q is the adit flow rate (L/day).
 317 Acidity removal rate (ARR) can be expressed according to the surface area ($\text{g/m}^2/\text{day}$) or
 318 volume ($\text{g/m}^3/\text{day}$) of the treatment. This operational parameter is typically used to control
 319 the efficiency and size of the remediation system, and can be obtained using the following
 320 expressions:

$$ARR = Q \cdot (NA_{in} - NA_{out}) \cdot A^{-1} \quad (3)$$

$$ARR = Q \cdot (NA_{in} - NA_{out}) \cdot V^{-1} \quad (4)$$

321 where Q is the flow rate (m^3/day), NA_{in} and NA_{out} are inflow and outflow net acidity (mg/L
 322 as CaCO_3 equivalents), and A (m^2) and V (m^3) are the treatment surface area and volume,
 323 respectively.

324 The narrow oscillations displayed by net acidity and acidity load values during the first
 325 stage (characterized by high metal content and low flow rate) could be considered the most
 326 representative state (or steady state) for the AMD at Mina Esperanza (Fig. 5). However,
 327 during the second stage (extreme metal content-high flow rate) the outmost pollution was

328 displayed with maximum *NA* (4.05 g/L as CaCO₃ equivalents) and *NAL* (1,548 kg/day as
329 CaCO₃ equivalents) 1.6 and 11.3 times higher than the average values characterizing stage
330 1 (Fig. 5). On the other hand, the important rainfall during the third stage and the absence
331 of a significant amount of evaporitic salts induced a dilution of the AMD, and subsequently
332 a decrease in the *NA* values comparing with stage 1 (Fig.5). Nevertheless, the *NAL* rose due
333 to the flow rate increment and achieved a maximum value 4.3 times higher than the average
334 values showed during stage 1.

335 Passive treatment systems are the most common choice to remediate AMD at abandoned
336 mining operations (Younger et al., 2002; PIRAMID Consortium, 2003; Watten et al., 2005)
337 This remediation option is typically restricted to flow rates lower than 100 L/s and it is
338 specially indicated for AMD long term remediation (from decades to centuries) due to its
339 economic and environmental sustainability (Johnson and Hallberg, 2005; Ayora et al.,
340 2013). The design of a passive treatment typically follows two consecutive steps: a) set a
341 characteristic pollution to treat, and b) up-scaling the system using a limiting operational
342 parameter. If at all possible, a year of AMD continuous monitoring is commonly advised as
343 a first step to be included in all AMD remediation designs (PIRAMID Consortium, 2003).
344 However, if the results belonging to the first year and a half of the current study were used
345 to design a remediation treatment, it would be clearly insufficient to address the large
346 fluctuations to come during the second and third stages. Therefore, a longer monitoring
347 period, never briefer than 5 years, should be considered a prerequisite for any passive
348 treatment system to be implemented in a dry Mediterranean climate.

349 Consideration should also be given to the influence of the observed AMD long-term
350 fluctuations at the time of up scaling a final passive treatment system. After some decades

351 of testing and experimentation, the most common passive treatment systems are expected to
352 achieve a distinctive metal removal, showing the following *ARR*: aerobic wetlands from 10
353 to 30 g/m²/day (Kruse et al., 2009; Kröpfelová et al., 2009; Szkokan-Emilson et al., 2014),
354 reducing and alkalinity producing systems between 25 and 30 g/m²/day (PIRAMID
355 Consortium, 2003; Marchand et al., 2010), dispersed alkaline substrate higher than 200
356 g/m²/day (Caraballo et al., 2011; Ayora et al., 2013), and oxidizing lagoon from 15 to 100
357 g/m²/day (Kruse et al., 2009; Macías et al., 2012). Although it is a common practice to
358 design compartmentalized systems to allow taking a section out of service for maintenance
359 (PIRAMID Consortium, 2003; Younger et al., 2014), passive treatment systems are
360 typically designed to have all their sections working together to achieve the desired *ARR*. If
361 the maximum *NAL* recorded in Mina Esperanza (1,548 kg/day as CaCO₃ equivalents) were
362 used to design a passive treatment system, the resulting system would be gigantic (i.e.,
363 using dispersed alkaline substrate, the current passive remediation technology with the best
364 *ARR*, the treatment surface area would be as exorbitant as 7,740 m²) and even worst, it
365 would be underused most of its operation time. A possible solution could be the
366 implementation of a modular system, comprising a main section designed to work under
367 common “working loads” (i.e., stage 1, 700 m² dispersed alkaline substrate treating a *NAL*
368 of 140 kg/day as CaCO₃ equivalents) and different “emergency” sections designed in
369 parallel to accommodate the *NAL* fluctuations when needed. These emergency sections
370 could be either active or passive depending on the specific needs and limitations of each
371 field site.

372 Another important lesson that should be extracted from the study of AMD long-term
373 fluctuations at Mina Esperanza is the need a continuous monitoring in dry Mediterranean

374 climate. This continuous supervision is essential for the early detection of *NAL* fluctuations
375 and subsequently, to activate the back up treatment sections. By the same token, the
376 traditional use of “pure passive treatment” (infrequent maintenance, low adaptability,
377 limited monitoring and electric energy free) to remediate AMD pollution in dry
378 Mediterranean climate should be discontinued. The next generation of “modular semi-
379 passive” treatment systems should grant a continuous monitoring of the *NAL* to be treated,
380 and a great adaptability to maximize the use of the different modular sections and
381 efficiently address the AMD oscillations.

382 Last but not least, climate change is directly impacting water resources and
383 hydrogeological/geochemical conditions on Earth and specifically on mining districts.
384 Changes in rainfall patterns, evapotranspiration, and hotter temperature have already been
385 documented in mining districts (Nordstrom, 2009). Mining sites with inadequate design,
386 management, or regulatory oversight will be more vulnerable to impacts of climate change
387 (Anaward, 2013). Therefore, the implementation of adaptive “modular semi-passive”
388 treatments is highly advisable to confront the impacts of climate change on an effective,
389 economic and sustainable way in the current mining sites with dry Mediterranean climate.
390 In this regard, it is highly encouraged to include (if economically possible) the effect of
391 climate change in the design of any future remediation systems. A possible action would be
392 to include a “climate change” safety parameter and increment the calculated maximum
393 operational margins by a factor of two.

394

395 **5. Conclusions**

396 The present study exposed the significant variations induced in acid mine drainage (AMD)
397 affected groundwater by long-term weather fluctuations. Specifically, three well-
398 differentiated hydrochemical stages were defined after more than 4 years monitoring an
399 AMD in a sulfide mining district with dry Mediterranean climate. The first stage displayed
400 high metal concentration and low flow rate, the second one showed an extreme metal
401 concentration and high flow rate, and finally the third one exhibited a mixed situation
402 between the two previous stages with high flow rate and medium-high metal
403 concentrations. Three different processes were considered as plausible mechanisms
404 responsible of the recorded long-term variability in AMD groundwater. However, the
405 following the three processes were proposed as the most influent ones: 1) pyrite and
406 enclosing rocks dissolution, responsible of the “background” metal concentration; 2)
407 evaporitic salts precipitation-redissolution, accountable for the storage and release of metal
408 pollution in the galleries during the inter-annual dry and wet periods, and 3) pluviometric
409 long term fluctuations, controlling the important variability of the AMD flow rate.

410 The intense metal load fluctuations presented in the current study have deep implications in
411 the design of AMD remediation strategies. On the light of these results, 5 years of AMD
412 continuous monitoring is strongly advised previous to the design of any AMD remediation
413 system in regions with dry Mediterranean climate. Additionally, these results encourage re-
414 assessing the use of more traditional and inflexible passive treatments to remediate AMD
415 pollution in dry Mediterranean climate should be reassessed. A possible solution could be
416 the implementation of modular systems, comprised by a main section designed to work
417 under common “working loads” coupled to a backup section designed in parallel to
418 accommodate the fluctuations on the acidity load when needed. The next generation of

419 “modular semi-passive” treatment systems should grant a continuous monitoring of the
420 pollution to be treated, and a great adaptability to efficiently address AMD long-term
421 fluctuations.

422

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430

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578

579 **FIGURE CAPTIONS**

580 Figure 1. Daily-accumulated rainfall (histogram, El Campillo weather station) and adit
581 water flow rate (circles connected by a dotted-line, Mina Esperanza) from March 2007 to
582 August 2011.

583 Figure 2. Time evolution of some pollutants concentration, water pH and flow rate. The
584 dotted areas correspond to the three stages proposed in this study.

585 Figure 3. Fe/S and Zn/Cu molar ratios versus adit AMD outflow during the study period.

586 Figure 4. A) Stage 3 principal component analysis. Alpha significance level 0.05. B)
587 Ferrous, ferric iron and discharge evolution during stages 2 and 3.

588 Figure 5. Adit outflow net acidity (g/L as CaCO₃ equivalents) and net acidity load
589 (Kg/day) during the study period.

590

591 **TABLES**

592 Table1. Selected weather parameters in the proximity of Mina Esperanza from 2001 to
593

594 **SUPPLEMENTARY INFORMATION**

595 Appendix 1. AMD evaporation experiment and geochemical model

596 Figure 1A. A) Mineral sequence predicted to form along the evaporation of Mina
597 Esperanza AMD. B) Aggregate of alunogel crystals (Al) surrounding prismatic crystals of
598 melanterite (Me) and gypsum (Gy).

599 Table A1. Summary of water physicochemical parameters and composition for the 61
600 samples comprising this study.

601 Table A2. PCA loadings matrix of the second stage.

602 Table A3. Chemical composition of the water and solids from the evaporation
603 experiment.

604 Table A4. Spearman correlation matrix of the 22 variables analyzed in the waters of the
605 second stage.

Fig. 2

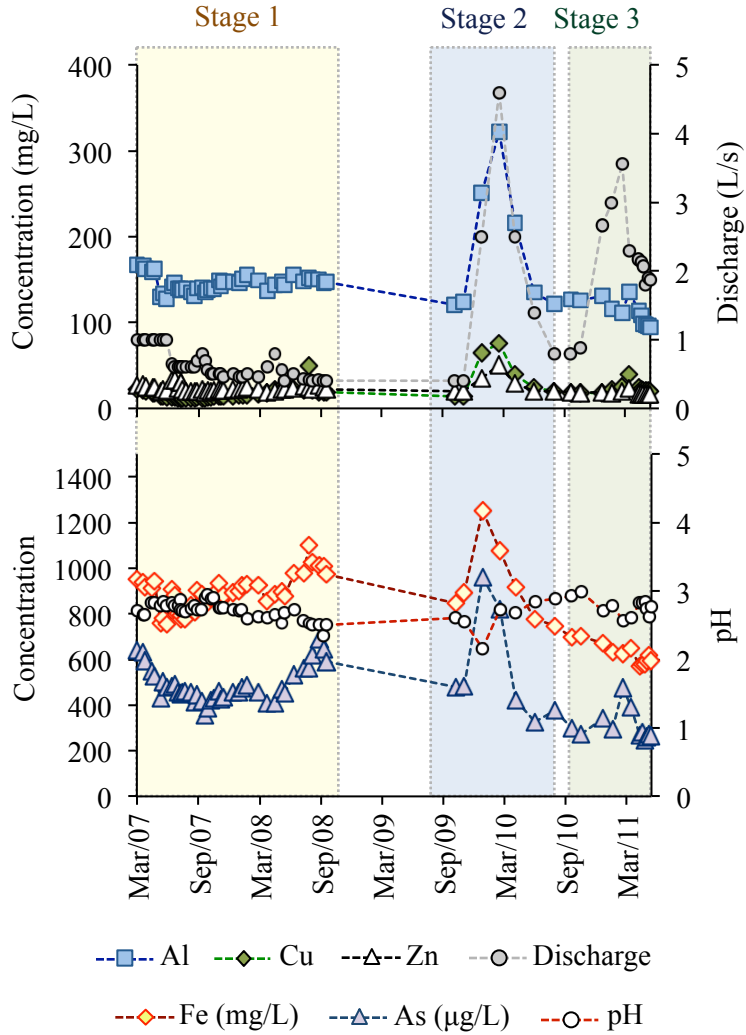


Figure 2. Time evolution of some pollutants concentration, water pH and flow rate. The dotted areas correspond to the three stages proposed in this study.

Fig. 3

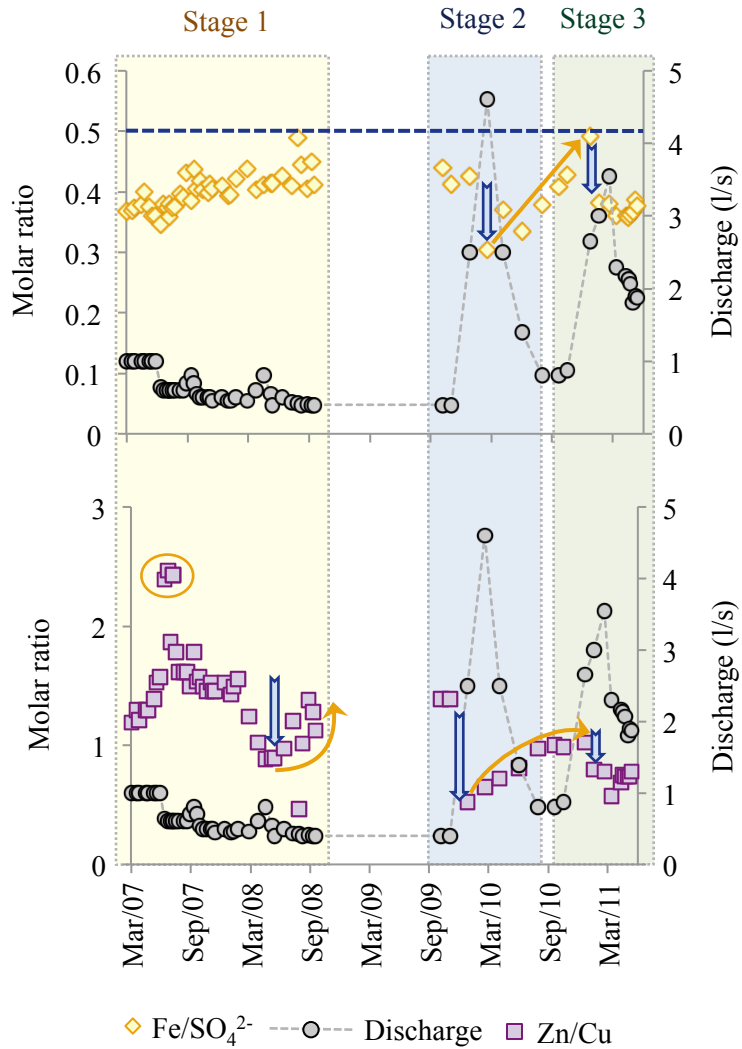


Figure 3. Fe/SO₄²⁻ and Zn/Cu molar ratios versus adit AMD outflow during the study period.

Fig. 4

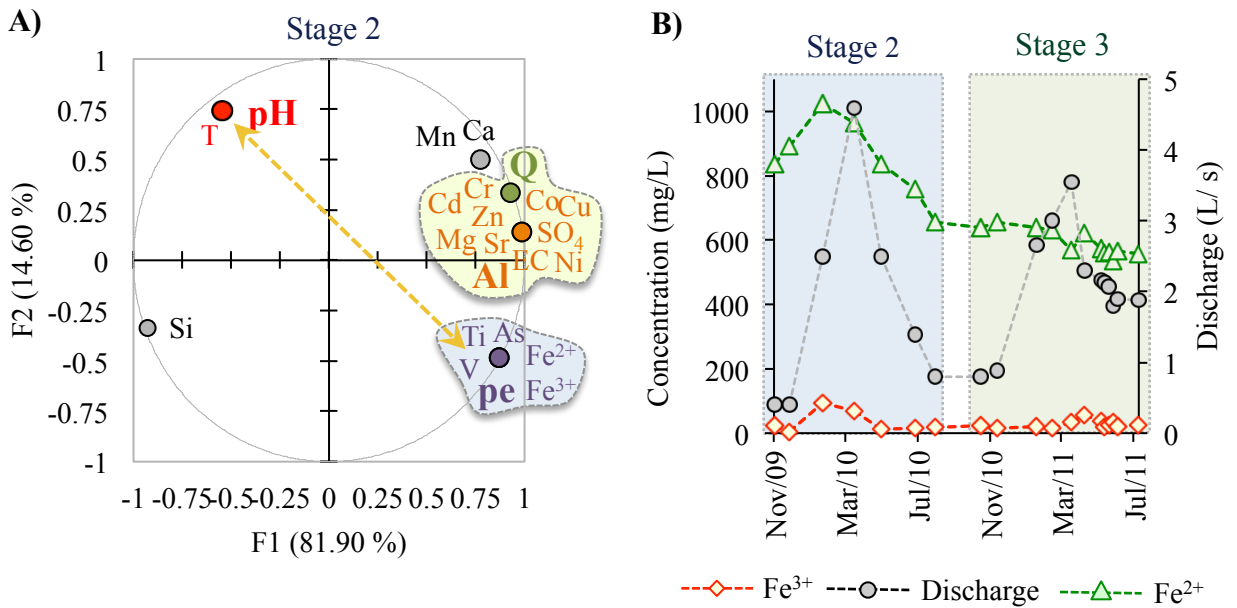


Figure 4. A) Stage 3 principal component analysis. Alpha significance level 0.05. Q = flow rate (L/s), EC = electrical conductivity, pe = redox potential. B) Ferrous, ferric iron and discharge evolution during stages 2 and 3.

Fig. 5

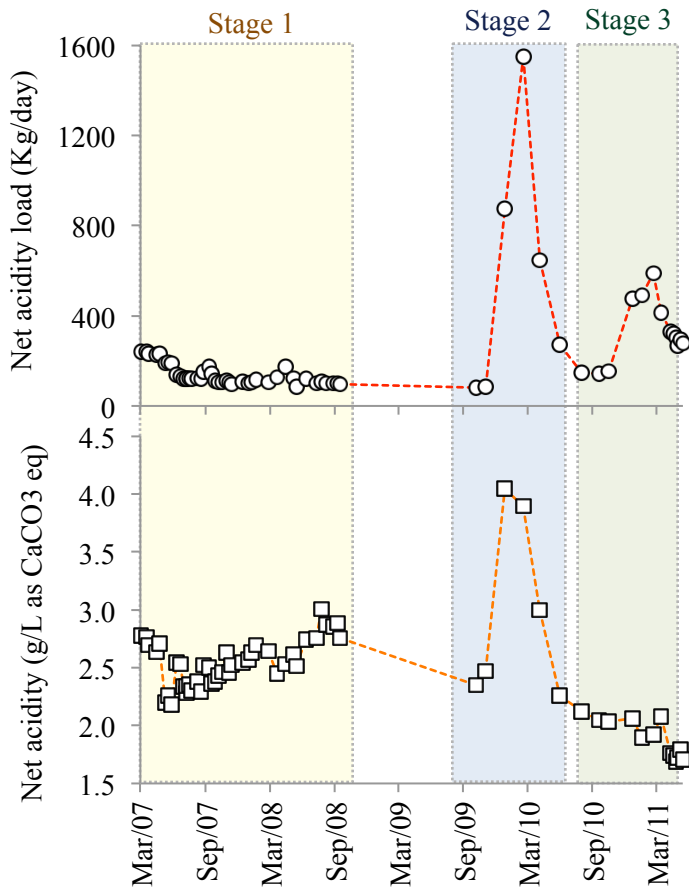


Figure 5. Adit outflow net acidity (g/L as CaCO₃ equivalents) and acidity load (Kg/day) during the study period.

Table 1. Selected meteorologic parameters in the proximity of Mina Esperanza for a decade of water years (2001- 2011)

Year	Ac. R. (mm)	T _{mean} (°C)	T _{St. Dev.} (°C)	T _{max./min} (°C)
2001	855.4	17.2	6.5	39.3/2.4
2002	750.4	17.0	5.9	38.2/0.0
2003	692.8	17.3	7.0	43.1/0.7
2004	784.4	17.2	7.0	42.3/0.9
2005	401.8	17.1	6.9	41.1/-2.4
2006	699.8	17.2	6.9	40.4/0.0
2007	758.2	16.9	6.1	41.6/-0.2
2008	662.8	16.6	6.3	39.2/0.1
2009	505.4	17.5	7.0	39.3/-1.4
2010	1223	16.7	7.4	40.6/-1.6
2011	1153.6	16.6	6.5	37.5/1.4
2001-11	771.6	17.0	6.7	43.1/-2.4

Ac. R. = Accumulated Rainfall