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6 ***Eucalyptus globulus* wood fractionation by autohydrolysis and**
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8 **organosolv delignification**
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Abstract: This work provides an assessment on the fractionation of *Eucalyptus globulus*, wood by sequential stages of autohydrolysis (to cause the solubilization of hemicelluloses) and organosolv pulping (to dissolve lignin, leaving solids enriched in cellulose). With this approach, valuable products (hemicellulose-derived saccharides, sulphur-free lignin fragments and cellulosic substrates with low contents of residual hemicelluloses) are obtained in separate streams, according to the biomass refinery approach. Autohydrolysis was carried out under optimized operational conditions, and the organosolv pulping step was performed using uncatalyzed ethanol-water solutions. The effects of the most influential operational variables (autohydrolysis severity, delignification temperature and ethanol concentration in the organosolv stage) on solid yield, solid composition, cellulose susceptibility and recovery of the various fractions was assessed using statistical method, which enabled the identification of the most favourable operational conditions.

Keywords: autohydrolysis, biorefinery, delignification, enzymatic hydrolysis, *Eucalyptus globulus*.

1. Introduction

Lignocellulosic Materials (LCM) are a basic resource for sustainable development. The biomass refinery approach, based on the selective separation of the major LCM components and their separate utilization for defined purposes, provides a valuable conceptual framework for an efficient utilization of LCM, whose fractionation can be achieved on the basis of the different properties of their structural components (cellulose, hemicelluloses and lignin), which are interpenetrated making part of a three-dimensional network.

In biorefineries, feedstocks are subjected to successive processing stages to extract value from each fraction, achieving an integral benefit with minimal or no waste generation, allowing the production of biofuels and/or chemicals (FitzPatrick et al., 2010; Michels and Wagemann, 2010; Zhang, 2008).

When biorefineries are designed to produce second-generation biofuels by enzymatic hydrolysis-fermentation, the fractionation stages have to enhance the susceptibility of the solid substrates to enzymatic hydrolysis, playing a role related to the ones of conventional pretreatments. The importance of pretreatments and their contribution to the operational costs of biorefineries have been pointed out (Eggeman and Elander, 2005; Mosier et al., 2005; Sun and Cheng, 2002). A convenient pretreatment should fulfill as many as possible of the following conditions: simple and economical structure; scalable to industrial size; limited requirements of energy, water and process chemicals; ability for breaking the structure of the feedstock; reduced polysaccharide losses; maximal production of valuable hemicellulose-derived products with limited generation of undesired degradation compounds; maximal production of valuable by-products from lignin; generation of processed, cellulose-containing solids with high susceptibility towards enzymatic hydrolysis; and minimal generation of processing wastes (Cara et al., 2006; Jørgensen et al., 2007; Mosier et al., 2005; Petersen et al., 2009; Pienkos and Zhang, 2009; Sun and Cheng, 2002).

Hemicellulose solubilization by autohydrolysis (or hydrothermal) processing with hot, compressed water has been proposed as the first step of biorefineries, owing to the

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5 possibility of obtaining a liquid phase rich in hemicellulose-derived sugars or oligomers
6 without causing significant dissolution of cellulose and lignin (Garrote et al., 1999).
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8 Operating under optimized autohydrolysis conditions, most hemicelluloses can be
9 recovered in liquid phase as xylooligosaccharides and xylose (Garrote et al., 2001),
10 whereas cellulose and lignin remain in solid phase, and could show enhanced susceptibility
11 to further fractionation (Kim et al., 2009; Laser et al., 2002). However, the cellulase
12 susceptibility of *Eucalyptus* wood autohydrolyzed under conditions leading to maximum
13 oligosaccharide production is limited (Romaní et al., 2010a).
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21 Ethanol-water solutions have been employed for LCM pulping (Díaz et al., 2004),
22 eventually in the presence of sulphuric acid (Zhu and Pan, 2010). This approach leads to
23 lignin fragments suitable for a variety of purposes (Pan et al., 2006), and to delignified
24 solids with improved susceptibility towards enzymatic hydrolysis. When this method is
25 applied to raw LCM, hemicelluloses can be just partially dissolved (Hallac et al., 2010), or
26 converted into sugar-dehydration products such as furfural or hydroxymethylfurfural (Pan
27 et al., 2007).
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34 Based on the above ideas, this work provides an experimental assessment on the
35 sequential processing of *Eucalyptus globulus* by autohydrolysis - organosolv delignification
36 for obtaining valuable products derived from hemicelluloses (hemicellulosic saccharides)
37 and lignin (solvent-soluble, sulphur-free lignin fragments), as well as cellulase-susceptible
38 solids suitable as substrates for the manufacture of second-generation bioethanol.
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45 **2. Materials and Methods**

46 **2.1. Raw Material**

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48 *Eucalyptus globulus* wood samples were obtained from a local pulp factory (ENCE,
49 Galicia, NW Spain), milled to pass an 8 mm screen, air-dried, homogenized in a single lot
50 to avoid differences in composition among aliquots, and stored in a dark and dry place until
51 use.
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56 **2.2 Analysis and Processing of the Raw Material**

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Eucalyptus globulus wood samples were milled to particle size less than 0.5 mm, and analyzed for extractives (TAPPI T-264-om-88m method), moisture (TAPPI T-264-om-88m method), and ashes (T-244-om-93 method). Additional samples were subjected to extractions and quantitative acid hydrolysis (QAH) (T-249-em-85 method). The liquid phase from QAH was assayed by HPLC for sugars (glucose, xylose, arabinose) and acetic acid, using a Refractive Index detector and a BioRad Aminex HPX-87H column, eluted with 0.01 M H₂SO₄ at a flow rate of 0.6 mL·min⁻¹. The solid residue from QAH was considered as Klason lignin.

The composition of the raw material (expressed in g/100 g wood in oven-dry basis ± standard deviation, based on four replicate determinations) was as follows: extractives 2.4 ± 0.15; ashes 0.23 ± 0.03; cellulose (as glucan), 44.39 ± 0.44; xylan 17.49 ± 0.65; arabinan 1.08 ± 0.05; acetyl groups 3.27 ± 0.23; and Klason lignin 27.67 ± 0.37.

Samples of autohydrolyzed *Eucalyptus globulus* wood (denoted AW) and solids resulting from autohydrolysis-delignification of *Eucalyptus globulus* (denoted ADW) were assayed for moisture and QAH using the same methods employed for the raw material.

2.3. Autohydrolysis and analysis of autohydrolysis liquors

Water and *Eucalyptus globulus* wood samples were mixed at a liquid to solid ratio (LSR) of 8 kg liquid/kg raw material (oven-dry basis). The mixture was reacted in a stainless steel reactor (Parr Instruments Company, Moline, IL) following the standard heating and cooling temperature profiles (Romaní et al., 2010b). Once the desired maximum autohydrolysis temperature (T_A) was reached, the media were immediately cooled, and aliquots of liquors were obtained by filtration. Based on reported data (Garrote and Parajó, 2002), operation was carried out at T_A of 185, 190, 195, 200 and 205 °C, in order to cover the range of severity conditions leading to significant generation of valuable hemicellulose-derived soluble compounds.

The effects achieved in a given non-isothermal autohydrolysis experiment can be measured in terms of severity (S_o), which includes the combined effects of temperature and reaction time along heating and cooling. S_o was defined by Lavoie et al. (2010) as:

$$So = \log Ro = \log [Ro_{HEATING} + Ro_{COOLING}] = \log \left[\int_0^{t_{MAX}} \frac{T(t) - T_{REF}}{\omega} dt + \int_{t_{MAX}}^{t_F} \frac{T'(t) - T_{REF}}{\omega} dt \right] \quad (1)$$

where Ro is the severity factor, t_{MAX} (min) is the time needed to achieve T_A (°C), t_F (min) is the time needed for the whole heating-cooling period, and $T(t)$ and $T'(t)$ represent the temperature profiles in heating and cooling, respectively. Calculations were made assuming the values reported in literature for ω and T_{REF} (14.75 °C and 100 °C, respectively). The So values calculated for the considered T_A were 3.35, 3.50, 3.64, 3.79 and 3.94.

AW samples were washed with distilled water and used to measure the solid yield of the autohydrolysis stage (Y_A , kg of AW/100 kg raw material, oven-dry basis). Other samples were employed for compositional analysis (see section 2.2). An aliquot of autohydrolysis liquors was filtered through 0.45 μ m membranes and used for direct HPLC determination of glucose, xylose, arabinose, acetic acid, hydroxymethylfurfural (HMF) and furfural (F), using the same method specified above. A second aliquot was subjected to quantitative posthydrolysis (by triplicate) with 4% w/w sulphuric acid at 121°C for 30 min, filtered through 0.45 μ m membranes, and analyzed by HPLC for oligomer determination. The results obtained in autohydrolysis are shown in Table 1.

2.4. Organosolv delignification of autohydrolyzed *Eucalyptus globulus* wood

AW samples were subjected to organosolv delignification with ethanol-water mixtures at a LSR of 8 g solution/g oven-dry AW for 1 h at the selected temperature. Time zero was taken when the system reached the preset temperature. When desired, the mixture was cooled, and the autohydrolyzed-delignified solids (ADW) were recovered and washed (first with ethanol/water and then with distilled water). After washing, ADW were used for gravimetric determination of the solid yield corresponding to delignification (Y_D , kg of ADW /100 kg AW, on dry basis), and a ADW sample was used for analysis (see section 2.2).

2.5. Enzymatic hydrolysis of ADW

Enzymatic hydrolysis assays of ADW was carried out at 48.5°C and pH= 4.85 (0.05 N citric acid-sodium citrate buffer) in 250 mL Erlenmeyer flaks with orbital agitation (150

rpm) using “Celluclast 1.5 L” cellulases and “Novozym” β -glucosidase, which were kindly provided by Novozymes (Madrid, Spain). The cellulase activity of “Celluclast 1.5 L” was measured by the Filter Paper assay, and the activity was expressed as Filter Paper Units (FPU) according to Ghose (1987). The β -glucosidase activity of “Novozym” was determined as International Units (IU) (Paquot and Thonart, 1982). The enzyme activities were 70.1 FPU/mL for “Celluclast 1.5 L” and 575 IU/mL for “Novozym”.

Enzymatic hydrolyses were carried out under the same conditions for ADW samples obtained under different conditions, to study the effects of processing on the cellulase digestibility. The conditions of enzymatic hydrolysis were LSR = 25 kg liquid/kg oven-dry ADW, cellulase/substrate ratio = 10.3 FPU/g oven-dry ADW, and β -glucosidase/cellulase ratio = 5 IU/FPU. The reaction time of enzymatic hydrolysis varied in the range 0-72 h. At the desired times, samples were withdrawn from the media, centrifuged, filtered and analyzed by HPLC for monosaccharides and acetic acid. Based on the typical variation pattern observed for the glucose concentration profiles (Garrote et al., 2008), the glucose concentration profiles determined for individual experiments were fitted to the following equation (Holtzapple et al., 1984):

$$CGC_t = CGC_{MAX} \frac{t}{t + t_{1/2}} \quad (2)$$

where CGC_t is the cellulose-to-glucose conversion achieved at time t , calculated as:

$$CGC_t = 100 \cdot \frac{G_t - G_{t=0}}{G_{POT}} \quad (3)$$

whereas CGC_{MAX} is the cellulose-to-glucose conversion predicted for an infinite reaction time, t is the enzymatic hydrolysis time (h), $t_{1/2}$ (h) is the time needed to achieve $CGC = CGC_{MAX}/2$, G_t is the glucose concentration (g/L) achieved at time t , $G_{t=0}$ is the glucose concentration at the beginning of the experiments, and G_{POT} represents the potential glucose concentration (corresponding to the stoichiometric conversion of the cellulose present in substrates into glucose). G_{POT} was calculated as:

$$G_{POT} = \frac{G_n \cdot 180}{100 \cdot 162} \cdot \frac{\rho}{LSR + 1 - \frac{KL}{100}} \quad (4)$$

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5 where G_n is the glucan content of ADW (kg glucan/100 kg ADW, on dry basis), 180/162 is
6 the stoichiometric factor, ρ is the density of the reaction medium (average value, 1005 g/L),
7 LSR is the liquid-to-solid ratio (25 kg liquid/kg ADW) and KL is the Klason lignin content
8 of ADW (kg Klason lignin/100 kg ADW).
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13 **2.6. Fitting of data**

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15 The experimental data were fitted to the proposed models using commercial
16 software (Microsoft Excel by Microsoft, U.S.A.)
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22 **3. Results and Discussion**

23 **3.1 Structure of the experimental design**

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25 The selection of the operational parameters employed in this work and their
26 variation ranges was based on the results obtained in preliminary experiments.
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28 Autohydrolysis was carried out at the severities indicated in Table 1, in order to achieve
29 fractionation effects (mainly related to the selective removal of hemicelluloses). The results
30 concerning the xylan contents of AW (from 10.9 to 2.73%) confirmed that the experimental
31 range considered was suitable for covering all the situations of practical importance (from
32 moderate up to extensive hemicellulose removal). As expected, due to the selectivity of the
33 autohydrolysis stage, the results concerning solid yield (81.8-72.4%) and the contents of
34 cellulose and lignin (in the ranges 54.3-61.4% and 26.3-32.0%) confirmed that both
35 components were almost quantitatively retained in solid phases upon autohydrolysis. On
36 the other hand, xylooligomers were the major hemicellulose-derived components present in
37 liquid phase, with minor amounts of glucooligosaccharides, oligosaccharide substituents,
38 monosaccharides, furans and acetic acid.
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50 In order to obtain a preliminary insight on the susceptibility of AW samples to
51 delignification, autohydrolyzed solids were processed with 60% ethanol under a variety of
52 operational conditions (see Table 2), operating at selected combinations of delignification
53 temperature (T_D in the range 175-200 °C) and delignification times (t_D in the range 60-120
54 min); and the resulting solids (ADW) were assayed for yield (Y_D) and composition.
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5 Additionally, ADW were assayed as substrates for enzymatic hydrolysis, and the cellulose
6 conversions into glucose were measured after 72 h (CGG₇₂). The experimental results
7 showed that significant fractionation could be achieved even in experiments performed
8 under the mildest delignification conditions assayed (175 °C, 60 min). In agreement with
9 literature (Pan et al., 2007), the reaction time (in the range assayed) showed a moderate
10 influence, whereas the results obtained under harsh conditions (200 °C for 120 min)
11 suggested the participation of lignin repolymerization reactions. Finally, the ADW
12 susceptibility to hydrolysis increased steadily with the severity of the operational
13 conditions.
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22 Based on the results achieved in these preliminary experiments, an experimental
23 plan (following a Doehlert design) was performed to assess the autohydrolysis-
24 delignification of *Eucalyptus* wood (see Figure 1). The structure of the experimental plan is
25 summarized in Table 3. The independent variables considered were the severity of the
26 autohydrolysis stage (denoted S_o , also measured by the normalized variable x_1), the
27 delignification temperature (T_D or x_2), and the ethanol concentration in the delignification
28 stage (C or x_3). The liquor to solid ratio in both autohydrolysis and delignification stages
29 was fixed in 8 g/g, and the delignification time in 1 h. The dependent variables include the
30 combined yield (denoted Y_C or y_1 , measuring the recovery of solids after autohydrolysis
31 and delignification, defined as kg ADW/100 kg raw material, oven dry basis), variables
32 measuring the composition of ADW samples (contents of glucan, xylan, acetyl groups and
33 Klason lignin, denoted variables y_2 to y_5 , respectively), and the susceptibility of ADW
34 towards enzymatic hydrolysis, which was measured by the two kinetic parameters of eq. 2
35 (CGC_{MAX} and $t_{1/2}$, or y_6 and y_7 in generalized nomenclature).
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48 For calculation purposes, the operational variables were expressed in terms of
49 dimensionless, normalized variables (x_1 , x_2 , and x_3) with variation ranges (-1,1), which are
50 linearly related to the corresponding independent variables (S_o , T_D or C) as follows:
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$$54 \quad x_1 = 2 \cdot \frac{S_o_i - S_{o_{me}}}{S_{o_{max}} - S_{o_{min}}} \quad (5)$$

$$55 \quad x_2 = 2 \cdot \frac{T_{D_i} - T_{D_{me}}}{T_{D_{max}} - T_{D_{min}}} \quad (6)$$

$$x_3 = 2 \cdot \frac{C_i - C_{me}}{C_{max} - C_{min}} \quad (7)$$

where the subscripts i, me, min and max correspond to the experiment considered, and to the mean, minimum and maximum values of the variation ranges, respectively.

The interrelationship between dependent and independent variables was established by empirical models following the generalized expression:

$$y_j = b_{0j} + \sum_i b_{ij}x_i + \sum_i \sum_k b_{ikj}x_i x_k \quad (8)$$

where y_j is the dependent variable considered (j : 1 to 12), x_i or x_k (i or k : 1 to 3, $k \geq i$) are the dimensionless, independent variables defined by equation (2), and $b_{0j} \dots b_{ikj}$ are the regression coefficients, calculated from the experimental data by multiple regression using the least-squares method. Table 4 shows the experimental values achieved for the experimental variables, whereas Table 5 lists the sets of regression coefficients $b_{0j} \dots b_{ikj}$ and their significance (based on the Student's t-test), as well as the statistical parameters measuring the correlation (R^2) and significance of models (based on the Fisher's F-test).

3.2. Organosolv delignification of AW and enzymatic hydrolysis of the resulting samples (ADW)

According with the data in Table 4, combined yield of autohydrolysis-delignification (Y_C or y_1) varied in the range 47.9 - 66.6 kg ADW/100 kg wood, the extreme values corresponding to experiments 10 and 12. Figure 2 shows the surface response calculated for Y_C as a function of the most influential operational variables. As a general trend, Y_C decreases with T_D , particularly in media containing low ethanol concentrations. So showed a related influence, but its effects were less marked.

The variation range determined for the ADW glucan content (variable G_n or y_2) was 70.3 – 86.9 kg glucan/100 kg oven-dry (o. d.) ADW (corresponding to experiments 4 and 6, respectively). Figure 3 shows the calculated dependence of y_2 on the most influential independent variables. The highest glucan content predicted by the model (for operation in media containing 50.2 kg ethanol/100 kg liquor) was 87.6 kg glucan/100 kg ADW,

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5 operating at $S_o = 3.50$ and $T_D = 202.7$ °C and. As a general pattern, the highest glucan
6 contents corresponded to samples treated at medium or high severities and at high T_D , with
7 a limited influence of the ethanol concentration.
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11 Considering ADW samples as potential substrates for biofuel production by
12 enzymatic hydrolysis, their high glucan contents are an advantage, as they increase the
13 potential glucose concentration for a given substrate loading. For example, the ADW
14 sample with highest cellulose content obtained in this work corresponds to a potential
15 glucose concentration 40% higher than the one reported in a related study (Romaní et al.,
16 2010a).
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20 As expected, ADW samples presented limited xylan contents (3.0 – 8.3 kg/100 kg),
21 which decreased with S_o . The rest of independent variables did not play a significant role
22 on this parameter. The lowest xylan content predicted by the models (for media containing
23 50.2 kg ethanol/100 kg) was 1.96 kg /100 kg ADW (operational conditions: $S_o = 3.89$, T_D
24 = 203 °C). This content corresponds to 93.4% xylan removal.
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28 The experimental trends found for variable y_4 (ADW content of acetyl groups) were
29 similar to the ones observed for the xylan content. The experimental range was 0.39 – 1.24
30 kg/100 kg, suggesting that this variable plays a role of limited importance in the whole
31 process.
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35 The Klason lignin content of samples (variable KL or y_5) varied in the range 10.2 –
36 22.7 kg/100 kg o. d. ADW. Figure 4 presents the surface responses calculated for KL as a
37 function of the most influential operational variables. In general terms, comparatively high
38 lignin contents are predicted for low values of T_D and S_o . For example, ADW with as much
39 as 31.5 kg KL/100 kg were predicted operating at $S_o = 3.35$ and $T_D = 172$ °C in media
40 containing 69.8 kg ethanol/100 kg liquor. Starting from the mildest operational conditions,
41 delignification was first improved by higher S_o and/or T_D , up to reach the minimum KL
42 (10.2 kg KL/100 kg ADW) under operational conditions defined by $S_o = 3.54$, $T_D = 199$ °C
43 (values calculated for $C = 64.0$ kg ethanol/100 kg mixture). Beyond these values, further
44 increases in S_o and/or T_D led to increased KL, a fact ascribed to lignin repolymerization
45 (Parajó et al., 1995). Considering the zone of the experimental domain defined by high S_o
46 and T_D , the models predicted the highest KL (29.6 kg/100 kg ADW) for samples treated at
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5 So = 3.94 and $T_D = 203$ °C (data calculated for media containing 50.2 kg ethanol/100 kg
6 liquor).
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9 All the ADW samples obtained in this work were susceptible towards enzymatic
10 hydrolysis. The data in Table 4 concerning variables y_6 (or CGC_{MAX}) and y_7 (or $t_{1/2}$)
11 confirmed that 10 in 15 samples subjected to autohydrolysis-delignification reached
12 CGC_{MAX} close to 100%, whereas the lowest CGC_{MAX} (65.7%) corresponded to the sample
13 treated under the mildest conditions. The second kinetic parameter ($t_{1/2}$) varied in the range
14 6.1 - 29.2 h. Comparatively, the enzymatic hydrolysis of autohydrolyzed *Eucalyptus*
15 *globulus* wood (not delignified) carried out under similar conditions (LSR = 20 kg/kg and
16 ESR = 10.3 FPU/g, So in the range 3.64 – 3.94) led to $t_{1/2}$ in the range 26 – 28 h and to
17 CGC_{MAX} in the range 54% - 98% (Romaní et al., 2010a). Obtaining autohydrolyzed solids
18 (not subjected to delignification) with an enzymatic digestibility similar to the ADW
19 samples considered in this work would entail aqueous processing under harsh conditions
20 ($So \geq 4.67$), which would lead to degradation of hemicellulosic sugars and partial cellulose
21 solubilization, worsening the integrated benefit of the whole raw material.
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34 **3.3. Recovery of components in ADW samples and enzymatic hydrolysis yield**

35 Based on knowledge of the composition of wood, and on the availability of
36 empirical models describing the dependences of ADW composition of combined yield on
37 the operational conditions, the recoveries of the various fractions in ADW can be directly
38 calculated. For this purpose, the following variables were defined:
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$$44 \text{ Glucan recovery} = \text{Rec}_{Gn} = Y_C \cdot \frac{Gn}{Gn_{RM}} \quad (9)$$

$$45 \text{ Klason lignin recovery} = \text{Rec}_{KL} = Y_C \cdot \frac{KL}{KL_{RM}} \quad (10)$$

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48 where the subscripts RM refer to the contents of the considered component in the raw
49 material, and the rest of variables have been defined before (see Table 3).
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52 The availability of suitable parameters for equations 2 and 8 enables a generalized
53 interpretation of the autohydrolysis-delignification-enzymatic hydrolysis process. Eq. 9
54 predicted glucan recoveries in the range 82.8% (operating under severe conditions, defined
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5 by $S_o = 3.94$, $T_D = 200$ °C and $C = 61.9$ kg ethanol/100 kg mixture) up to 100% (for
6 samples treated under a variety of conditions). On the other hand, the recovery of Klason
7 lignin in processed samples reached its minimum predicted value (19.1%) under conditions
8 defined by $S_o = 3.56$, $T_D = 198$ °C and $C = 59.5$ kg ethanol/100 kg liquor, and its maximum
9 predicted value (65.6%) operating at $S_o = 3.94$, $T_D = 203$ °C and $C = 50.2$ kg ethanol/100
10 kg liquor.
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16 The high recovery of cellulose in processed solids, together with the extensive
17 removal of hemicelluloses and lignin from solid phase, confirmed the suitability of the
18 approach considered in this study for an efficient fractionation of *Eucalyptus globulus*
19 wood.
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23 In order to assess the fractionation effects achieved, Figure 5 shows the results
24 calculated for variables Rec_{Gn} , Rec_{KL} , CGC_{24} (cellulose to glucose conversion after 24 h)
25 and CGC_{72} (cellulose to glucose conversion after 72 h) along the most favourable zone of
26 the experimental domain (defined by S_o in the range 3.65 - 3.94 and T_D in the range 180 -
27 200 °C. For the sake of simplicity, the results have been calculated for concentration media
28 containing the intermediate ethanol concentration (60 kg ethanol/100 kg liquor). Under
29 these conditions, cellulose was almost or totally retained in ADW, whereas the degree of
30 lignin removal reached values up to 81%, CGC_{24} was higher than 80%, and CGC_{72} was
31 close to 100%.
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40 In order to highlight the fractionation effects achieved under suitable conditions and
41 the susceptibility of the resulting samples to hydrolysis, Figure 6 shows the ranges
42 calculated for the mass flows of fractions (or compounds) for the range of operational
43 conditions considered in Figure 5. Stream B (autohydrolysis liquors) accumulated 67 –
44 75% of the initial hemicelluloses in the form of saccharides (mainly of oligomeric nature).
45 These latter are valuable, as xylooligosaccharides find direct application in pharmaceutical
46 and food industries (Moure et al., 2006) or can be hydrolyzed to xylose and further
47 converted by chemical methods (for example, hydrogenation to xylitol), or by fermentation
48 (for example, to lactic acid or ethanol). Stream C (pulsing liquors) contained up to 67% of
49 the initial lignin. Stream E (enzymatic hydrolysis media after 72 h) contains glucose at a
50 yield in the range 31.1 – 43.6 kg / 100 kg de raw material.
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7 Comparative advantages can be found for operational conditions defined by $S_o = 3.64$, T_D
8 $= 198\text{ }^\circ\text{C}$, $C = 60\text{ kg ethanol/100 kg liquor}$, and duration of enzymatic hydrolysis 72 h.
9
10 These conditions led to the following yields: 18.1 kg of oligomers, as monomers, and
11 sugars in stream B/100 kg o. d. wood, 17.9 kg of soluble lignin in stream C/100 kg o. d.
12 wood, and 41.9 kg glucose/100 g o. d. wood. As a whole, the processing of 100 kg of o. d.
13 wood would result in the recovery of 77.9 kg of valuable fractions or products in three
14 separate streams, each fraction being suitable for the individual manufacture of fuels and/or
15 chemicals.
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23 **4. Conclusions**

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25 The processing method enabled an efficient fractionation of *Eucalyptus globulus*
26 wood. Hemicelluloses were converted into mono- and oligosaccharides, whereas
27 autohydrolyzed wood was extensively delignified using uncatalyzed ethanol-water
28 solutions. Autohydrolyzed - delignified wood samples (ADW) obtained under a variety of
29 operational conditions were highly susceptible to enzymatic hydrolysis. The availability of
30 empirical models giving the interrelationship of selected variables (measuring the combined
31 yield and the composition of ADW, as well as the kinetic parameters involved in enzymatic
32 hydrolysis) allowed a generalized interpretation of data, as well as the identification of
33 conditions leading to favourable fractionation and enzymatic hydrolysis yield.
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43 **Acknowledgements**

44
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47 production" (reference 08REM002383PR) and “Hemicellulosic bioethanol: compatibility
48 with the *kraft* process” (reference 09REM003383PR).
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Table 1. Data obtained in wood autohydrolysis: solid yield (Y_A), composition of autohydrolyzed wood (AW) and composition of autohydrolysis liquors.

So	3.35	3.50	3.64	3.79	3.94
Y_A (kg AW/100 kg raw material, on dry basis)	81.8	74.2	74.0	73.3	72.4
Autohydrolyzed <i>Eucalyptus globulus</i> wood composition (kg/100 kg AW, on dry basis)					
Gn (glucan)	54.3	57.5	58.7	61.4	60.6
Xn (xylan)	10.9	6.18	5.17	4.34	2.73
AcG (Acetyl groups)	1.73	0.98	0.86	0.36	0.37
KL (Klason lignin)	26.3	30.8	32.8	32.0	32.2
Liquid phase composition (g/L)					
GO (Gluco-oligomers¹)	0.53	0.36	0.86	0.92	0.98
XO (Xylo-oligomers¹)	8.60	12.5	14.6	14.0	10.2
ArO (Arabinosyl moities in oligomers¹)	0.41	0.42	0.00	0.00	0.00
AcGO (Acetyl groups in oligomers¹)	1.83	2.88	2.71	2.74	2.20
G (Glucose)	0.23	0.47	0.12	0.16	0.20
X (Xylose)	0.58	1.83	2.73	4.16	5.60
Ar (Arabinose)	0.29	0.28	0.46	0.56	0.44
AcH (Acetic acid)	0.20	0.20	0.62	0.85	1.23
HMF (Hydroxymethylfurfural)	0.01	0.02	0.03	0.07	0.09
F (Furfural)	0.07	0.14	0.22	0.56	0.78

¹: expressed as monomer equivalents

Table 2. Results obtained in preliminary experiments of autohydrolyzed wood pulping (performed in pulping media containing 60 weight percent ethanol)

(Nomenclature: AW: autohydrolyzed wood; ADW: autohydrolyzed delignified wood; So: severity, dimensionless; T_D: delignification temperature, °C; t_D: delignification time, min; Y_D: delignification yield, kg ADW/100 kg AW, on dry basis; Gn: glucan content, kg Gn/100 kg ADW, on dry basis; Xn: xylan content, kg Gn/100 kg ADW, on dry basis; KL: Klason lignin content, kg KL/100 kg ADW, on dry basis; CGC₇₂: Cellulose conversion into glucose achieved after 72 h, kg glucose/ 100 kg potential glucose)

Experimental conditions				Experimental results				
Exp	So	T _D	t _D	Y _D	Gn	Xn	KL	CGC ₇₂
P01	3.64	175	60	75.4	74.5	2.10	20.2	39.4
P02			120	72.8	77.3	3.16	17.5	46.8
P03		200	60	68.6	81.3	4.24	14.0	54.1
P04			120	67.2	85.2	3.84	10.7	53.9
P05	3.79	175	60	75.8	74.8	3.92	17.2	47.1
P06			120	73.0	77.8	3.17	14.5	57.4
P07		200	60	70.0	83.7	2.70	13.1	58.2
P08			120	66.6	87.1	2.53	10.3	58.3
P09	3.94	175	60	76.7	77.3	2.80	16.2	47.5
P10			120	72.9	78.1	2.93	17.2	49.6
P11		200	60	70.1	83.0	2.46	13.0	54.9
P12			120	68.2	83.6	2.57	11.8	60.9

Table 3. Variables involved in the experimental design considered in this work (AW: autohydrolyzed wood, ADW: autohydrolyzed delignified wood, o.d.b.: on dry basis).

Nomenclature		Variable	Value or range		Units
Fixed variables					
LSR _A		Liquid to solid ratio in autohydrolysis	8	kg liquid/ kg raw material, o.d.b.	
LSR _D		Liquid to solid ratio in delignification	8	kg liquid/ g AE, o.d.b.	
t _D		Isothermal delignification time	1	h	
Independent variables					
So	x ₁	Severity of hydrothermal treatment	3.35-3.94	Dimensionless (So = Log Ro, with Ro in min)	
T _D	x ₂	Delignification temperature	172-203	°C	
C	x ₃	Ethanol concentration in pulping media	48-72	kg ethanol/100 kg liquor	
Dependent variables					
Y _C	y ₁	Combined yield	kg ADW/100 kg raw material, o.d.b.		
Gn	y ₂	Glucan content of ADW	kg glucan/100 kg ADW, o.d.b.		
Xn	y ₃	Xylan content of ADW	kg xylan/100 kg ADW, o.d.b.		
AcG	y ₄	Acetyl groups content of ADW	kg acetyl groups/100 kg ADW, o.d.b.		
KL	y ₅	Klason lignin content of ADW	kg Klason lignin/100 kg ADW, o.d.b.		
CGC _{MAX}	y ₆	Maximum cellulose-to-glucose conversion in enzymatic hydrolysis	kg glucose/ 100 kg potential glucose		
t _{1/2}	y ₇	Time to achieve CGC _{MAX} /2 in enzymatic hydrolysis	h		

Table 4. Operational conditions considered (expressed in terms of dimensional and dimensionless independent variables) and experimental results obtained for dependent variables y_1 to y_7 (see Table 3 for definitions and units).

Exp	Independent variables			Dimensionless, normalized independent variables			Dependent variables						
	So	T _D (°C)	C (% ethanol)	x ₁	x ₂	x ₃	y ₁	y ₂	y ₃	y ₄	y ₅	y ₆	y ₇
1	3.94	188	60	1	0	0	53.5	77.7	3.48	0.42	20.6	100	10.5
2	3.35	188	60	-1	0	0	57.7	70.7	8.34	1.24	18.1	65.7	24.8
3	3.79	203	60	0.5	0.866	0	50.0	79.0	4.20	0.40	17.8	100	8.0
4	3.50	172	60	-0.5	-0.866	0	65.6	70.3	6.64	0.68	22.7	93.9	29.2
5	3.79	172	60	0.5	-0.866	0	56.2	77.8	4.60	0.75	17.9	71.5	22.0
6	3.50	203	60	-0.5	0.866	0	57.4	86.9	5.32	0.65	10.2	100	8.4
7	3.79	193	72	0.5	0.289	0.817	49.6	84.9	4.59	0.44	13.6	100	8.7
8	3.50	182	48	-0.5	-0.289	-0.817	61.2	78.1	5.90	0.82	17.6	100	17.6
9	3.79	182	48	0.5	-0.289	-0.817	63.3	81.0	3.88	0.55	16.8	100	7.1
10	3.64	198	48	0	0.577	-0.817	47.9	85.8	2.99	0.39	13.2	100	6.1
11	3.50	193	72	-0.5	0.289	0.817	62.7	81.0	6.03	0.84	12.0	98.6	23.3
12	3.64	177	72	0	-0.577	0.817	66.6	77.6	4.86	0.71	15.0	85.5	24.8
13	3.64	188	60	0	0	0	52.5	82.6	4.90	0.68	11.5	100	16.0
14	3.64	188	60	0	0	0	51.3	81.9	5.05	0.83	12.2	100	16.6
15	3.64	188	60	0	0	0	49.5	82.6	4.69	0.68	11.7	100	15.3

Table 5. Regression coefficients and statistical parameters measuring the correlation and significance of the models.

Parameter	y ₁	y ₂	y ₃	y ₄	y ₅	y ₆	y ₇
b₀	51.09***	82.38***	4.878***	0.7302***	11.80***	1.000***	15.98***
b₁	-4.534*	2.523**	-2.044***	-0.3120***	1.073***	0.05947	-7.678***
b₂	-6.688**	5.542***	-0.5806**	-0.1354*	-3.635***	0.09483	-9.716***
b₃	1.327	-0.3119	0.5543**	0.04723	-1.421***	-0.03236	5.304**
b₁₁	4.514	-8.180***	1.033**	0.1031	7.518***	-0.1714	1.644
b₂₂	1.125	-8.918***	0.5290	-0.1860	7.166***	0.1291	3.912
b₃₃	-9.722	3.803	0.1657	-0.01332	-1.061	-0.03727	-3.840
b₁₂	6.750	-2.465	0.06686	-0.1817	4.630***	-0.05820	0.6747
b₁₃	3.524	1.307	1.325**	0.06334	0.2682	0.1376	-2.166
b₂₃	8.377*	1.196	-0.5329	-0.1379	1.292**	0.01778	-2.634
R²	0.806	0.963	0.969	0.873	0.995	0.673	0.948
F	2.30	14.6	17.4	3.82	110	1.14	10.2
Significance level	92%	> 99%	> 99%	98%	> 99%	< 80%	> 99%

** Coefficients significant at the 99% confidence level; ** Coefficients significant at the 95% confidence level; * Coefficients significant at the 90% confidence level

1 **FIGURE LEGENDS**
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4 Figure 1: Scheme of the autohydrolysis-delignification process considered in this work.
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6 Figure 2: Calculated dependence of the combined yield (Y_C , kg ADW/100 kg raw
7 material, on dry basis) on autohydrolysis severity (S_o , dimensionless) and
8 delignification temperature (T_D , °C). Results calculated from media containing
9 60 kg ethanol/100 kg liquor.
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13 Figure 3: Calculated dependence of glucan content of ADW (G_n , kg glucan/100 kg
14 ADW, on dry basis) on autohydrolysis severity (S_o , dimensionless) and
15 delignification temperature (T_D , °C). Results calculated from media containing
16 60 kg ethanol/100 kg liquor.
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21 Figure 4: Calculated dependence of Klason lignin content of ADW (KL , kg Klason
22 lignin /100 kg ADW, on dry basis) on autohydrolysis severity (S_o ,
23 dimensionless) and delignification temperature (T_D , °C). Results calculated from
24 media containing 60 kg ethanol/100 kg liquor.
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28 Figure 5: Contour lines calculated for variables Rec_{G_n} (kg de G_n in ADW/100 kg G_n in
29 raw material, on dry basis), Rec_{KL} (kg KL en ADW/100 kg KL in raw material,
30 on dry basis), CGC_{24} (cellulose to glucose conversion after 24 h) and CGC_{72}
31 (cellulose to glucose conversion after 72 h). Results calculated from media
32 containing 60 kg ethanol/100 kg liquor.
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37 Figure 6: Summary of material balances for selected ranges of the most influential
38 independent variables.
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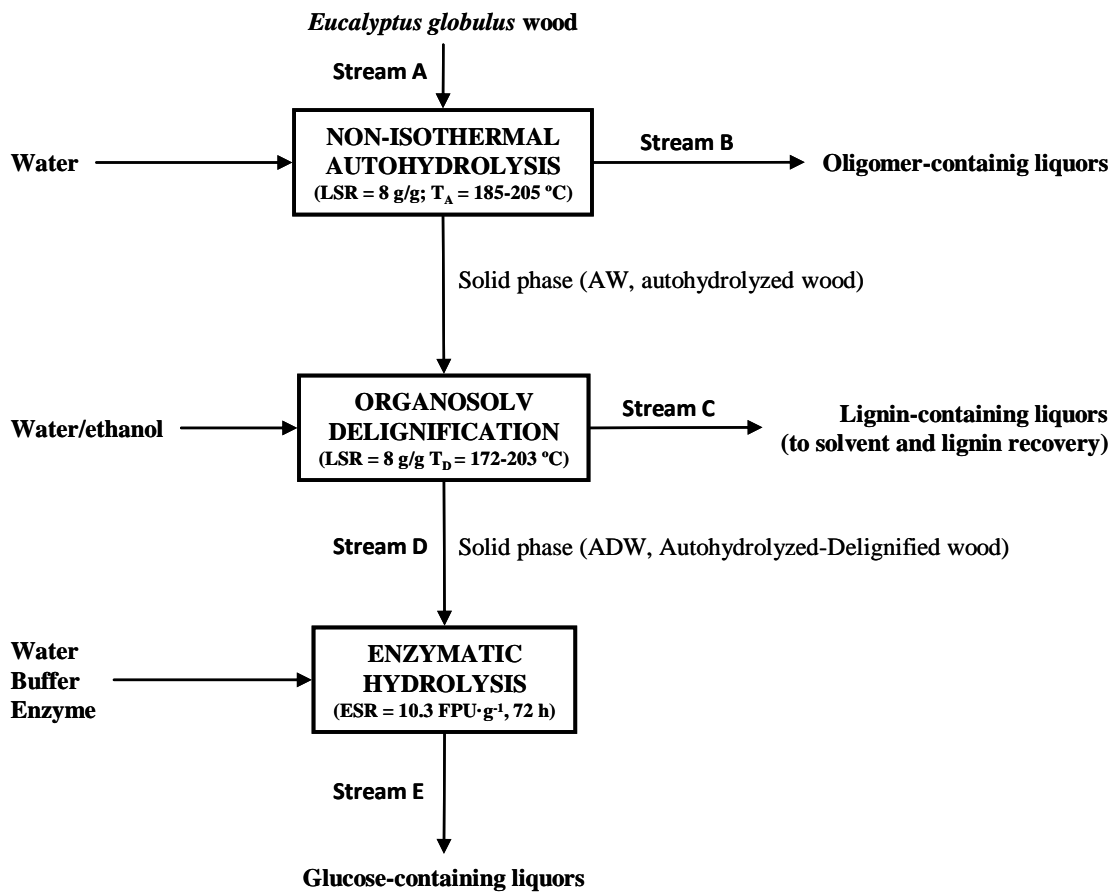


Figure 1

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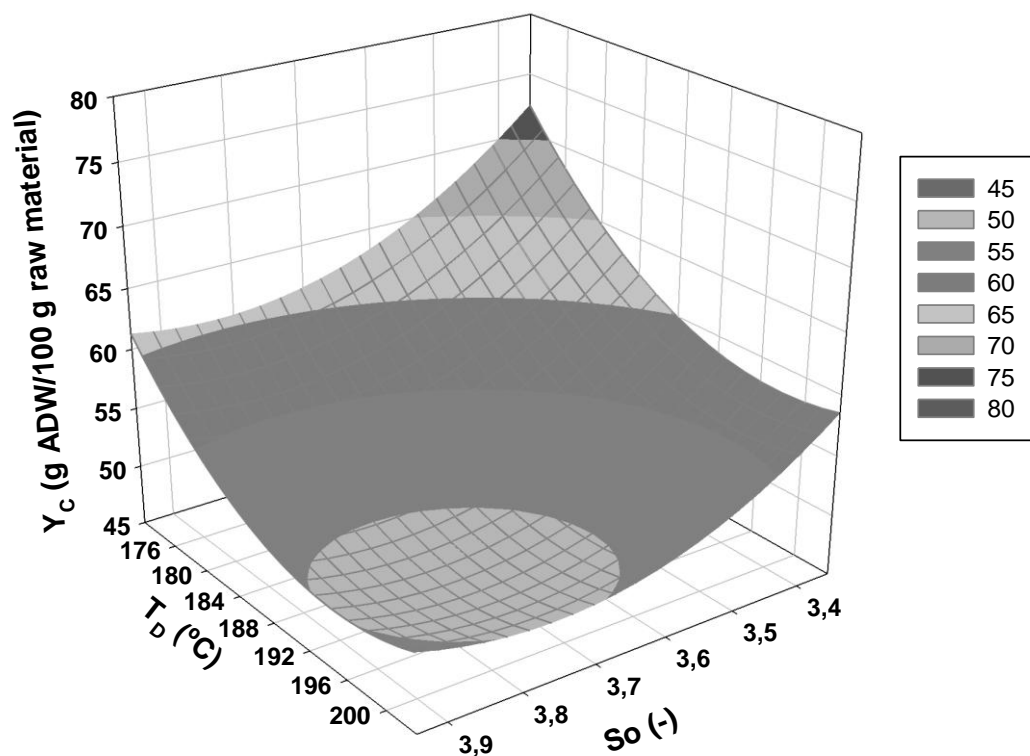


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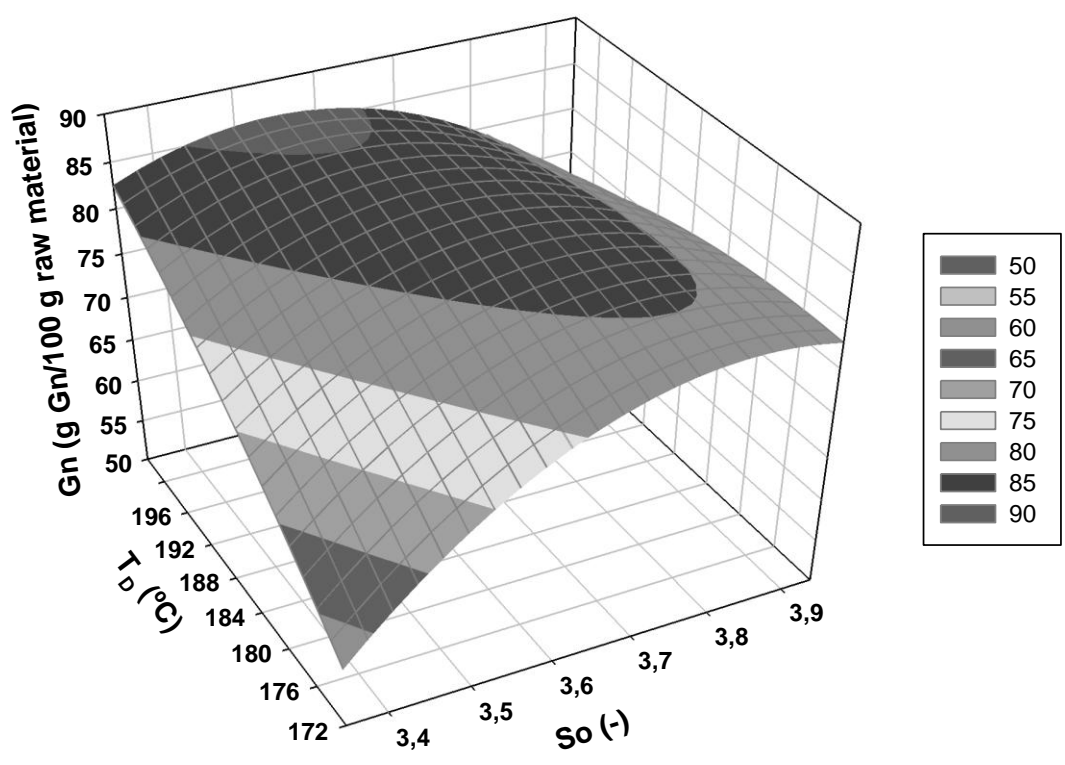


Figure 3

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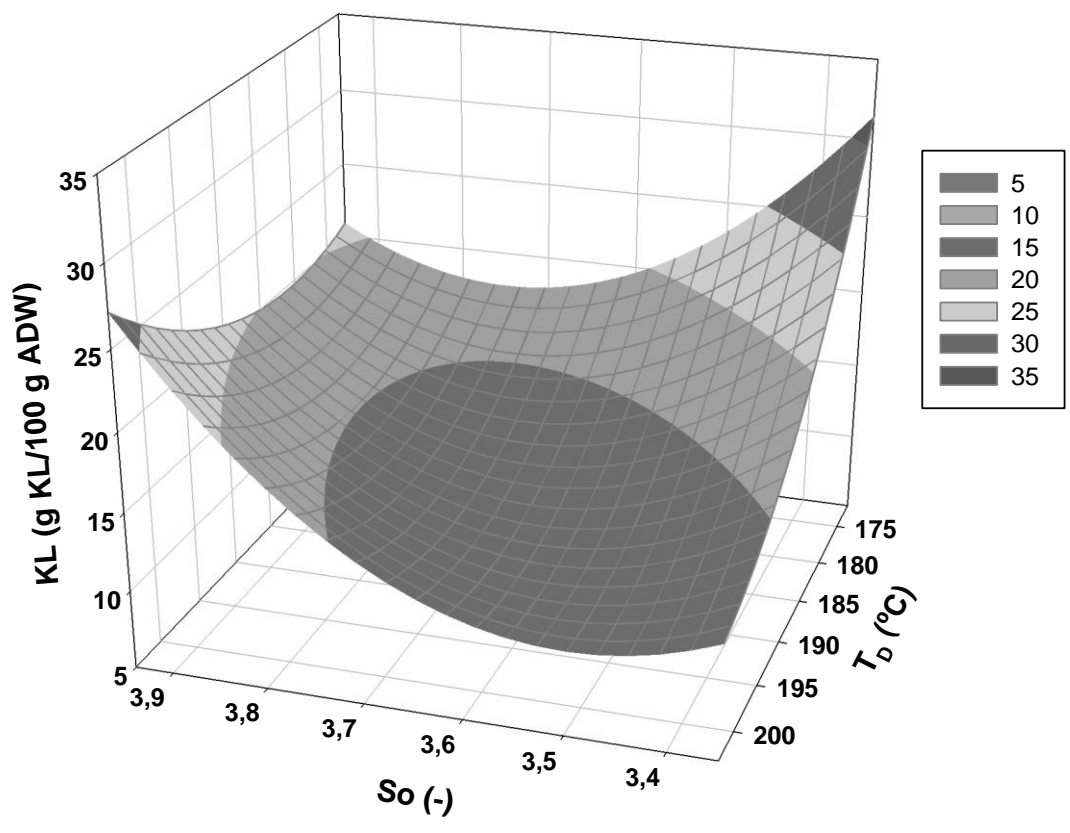


Figure 4

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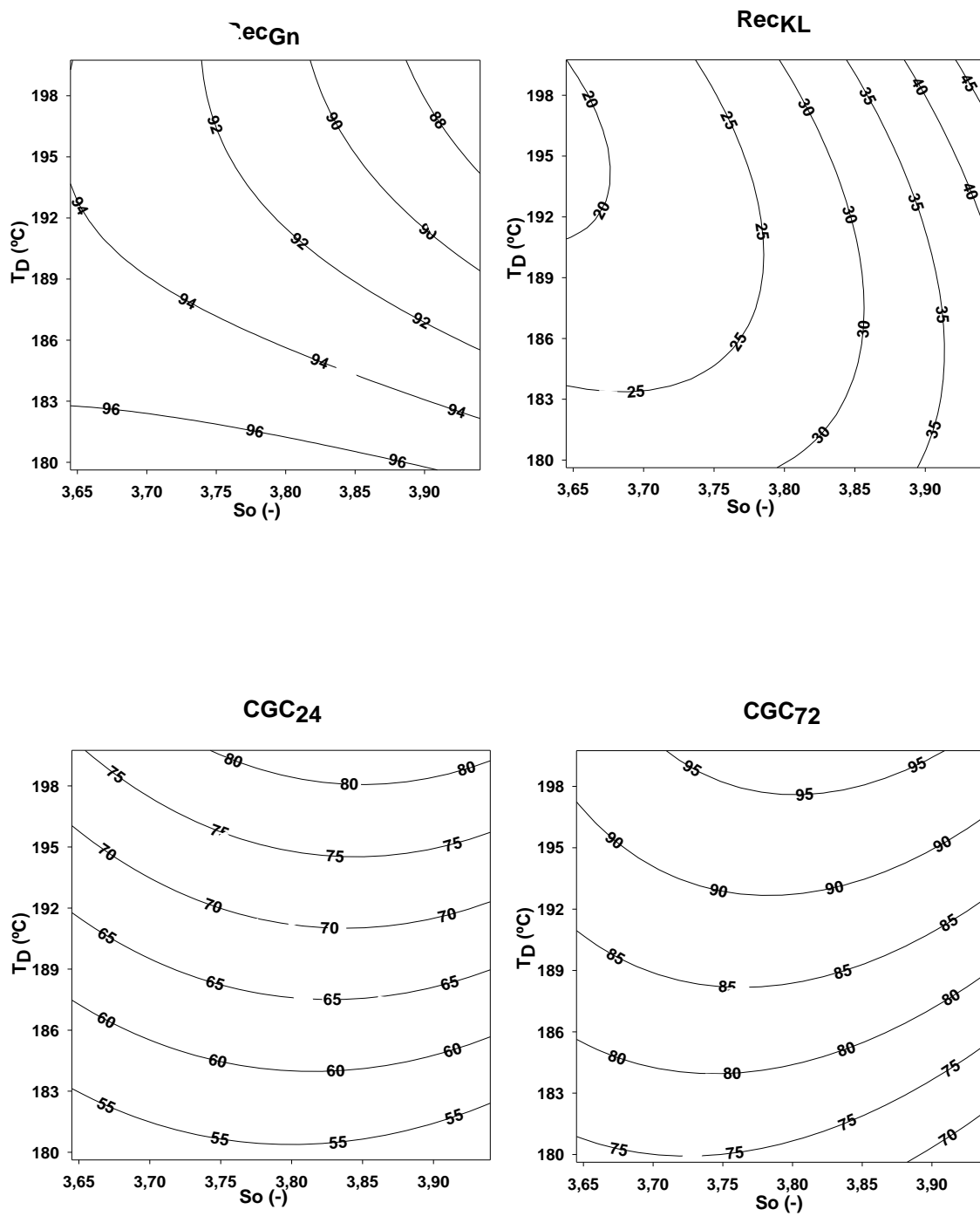


Figure 5

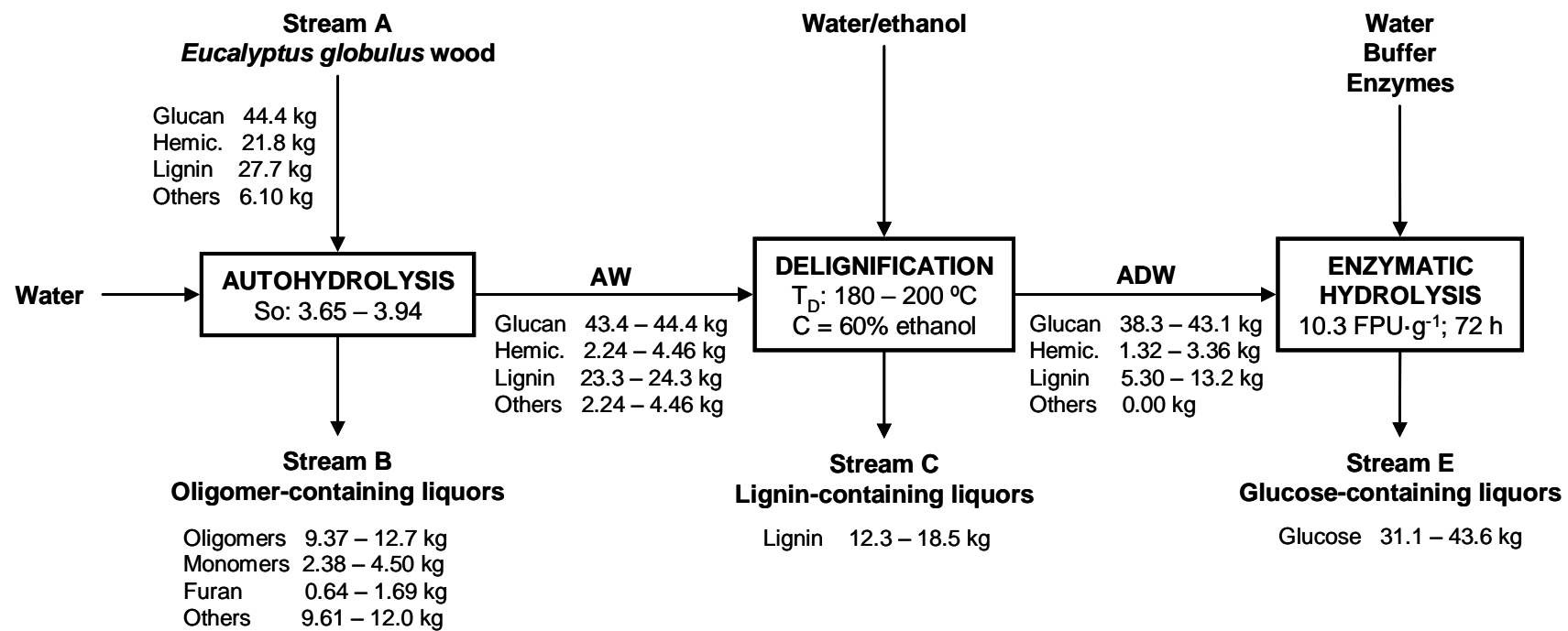


Figure 6